

8 May 2025 24-0468

Ku-ring-gai Council 818 Pacific Highway, Gordon NSW 2072 Attention Michael Cutajar

Dear Michael,

RE: Civil Engineering Design Review and Flood Impact Assessment Certification for Norman Griffith Oval Refurbishment.

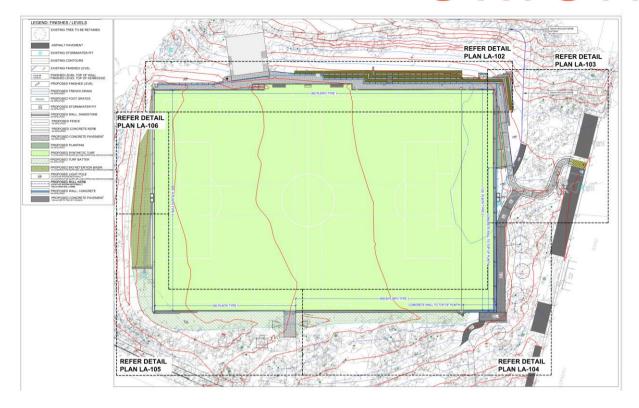
We certify that we have prepared the flood impact assessment and review of the stormwater design of the proposed **Norman Griffiths Oval Refurbishment works** as shown on the list of drawings attached in accordance with the intent of following:

- Provision of an independent review of the stormwater design on behalf of Council to confirm the performance of the OSD system and that the storage capacity is sufficient for the 100 Year storm event to not surcharge onto the oval surface
- Council request the documentation that assures the community that this sports field will work as a detention basin and is floodproof. This will require a review of the flood assessment and modelling of the entire system.

Orion have provided the Flood Impact Assessment and the stormwater review report (refer appendix A) and provided the overland flowpath in the south east corner of the oval is provided and the design detention storage is provided via the provision of stable gravel storage with the compliant void ratio, then the performance of the Oval works with respect to not making the flood conditions worse, also the condition of the detention storage not surcharging in the 100 year storm will be met, subject to suitable maintenance of the stormwater system for the oval.







The D&C contractor is to confirm that the works have been completed in accordance with the stamped approved drawings and the overland flow path additions and levels provide to ensure the design complies.

Yours Faithfully

Orion Consulting Engineers Pty Ltd

Technical Director | Stephen Brain

BE Civil (hons), MIE Aust, CPEng, NER 474 118, PRE0000910, DEP0001178, PDP0000390





Appendix A – Flood Impact Assessment and Stormwater Detention System Review Report



Detailed Flood Impact
Assessment and independent
sign off

Norman Griffiths Oval Upgrade Works



Prepared by Orion Group for



Ku-ring-gai Council September 2024

24-0468





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Document Control

Revision	Prepared by:	Approved by:	Date:	Description:
001	Stephen Brain	Stephen Brain	29/8/2024	Issue for review
002	Stephen Brain	Stephen Brain	19/9/2024	Independent review issue

theoriongroup.au September 2024 I i

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1. Executive Summary

Preliminary Flood impact Report

. Need for an independent sign off

Council have not had an independent flood specialist confirm the design will work as a detention tank nor be flood proof.

Council requires an independent sign off that the completed Norman Griffiths Oval development will work as a detention system, and that the oval is not inundated in storm events up to the 1% AEP event.

Council commissioned Orion to provide an initial flood and drainage modelling review which identifies compliance with catchment assessment practice flood modelling and detention modelling.

Orion undertook to identify areas of additional work required for the TUFLOW flood model using the proposed oval development and the drains model to enable a clear analysis of the predevelopment flood condition versus the post development condition.

This work stage included a review of the detention volume provided in the subsurface system and any amplification recommended.

Detailed Flood Assessment

Stage 2. In This report Orion has provided an independent analysis to allow sign-off of the Normal Griffiths oval works in terms of its flood protection level, and the compliance of the on-site stormwater detention volume provided in the design and that constructed by close analysis of the Tuflow model and drains models as recommended in stage 1 and close analysis of the as built site records.

PMF Analysis

Stage 3. Provide PMF analysis in TUFLOW and afflux analysis to identify the impact caused by the works under construction

Outcome

As a result of our analysis, we are willing to sign off on

 the diversion of the overland flow flood risk in the 1% AEP storm event from the upstream catchment east of Lofberg Road Quarry creek around the oval site, provided





- a. the 3m wide concrete pathway specified at the levels specified is constructed in accordance with our markups to ensure sufficient capacity is provided for the overflow occurring in this flood event.
- b. The diversion wall is constructed to the top of wall levels we have specified
- c. The drainage at the base of the bleachers is installed and maintained.
- 2. The compliance of the on site detention storage under construction provided
 - a. the specified volume is achieved which will remain below the playing surface level in the 1% AEP storm event.
 - b. We can rely on the site based testing results provided by JK geotechnical engineers on the void ratio for the detention storage rockfill at 36% versus the 40% specified in the Stamped approved drawings.
- 3. Our recommendation to address the settlement risk of the field drainage media and playing surface bedding media is addressed by the addition of a bidim later between the detention storage rockfill and the bedding layer for the shockpad and playing surface to limit settlement of the playing surface via material loss from the bedding layer into the detention storage layer, or a suitable guarantee is provided that the contractor will make good on settlement defect for the period of the defects liability period.



2. Introduction

Orion has been engaged by Kuring-Gai Council to provide flood impact advice for the Norman Griffiths Oval Redevelopment works

As the analysis completed to date did not have detailed modelling of the proposed works in QGIS and modelling in Tuflow, we were not able to assess the HGL level in front of the wall, other than identifying that the overflow over Lofberg road is over 2cum/s and the capacity of the void behind the wall constructed will not accommodate over 2 cum/s.

The options considered were

- 1. widening the overflow channel
- 2. raising the proposed retaining wall west of Lofberg Road.
- 3. allowing flow over the wall and onto the oval in storms less than the 1% AEP event.
- 4. Tuflow confirmation recommended for upstream effects of the constructed wall and to assess the overland flow path capacity.

Our flood preliminary advice report for the proposed oval redevelopment works included.

- Reviewing existing information including Council flood maps and studies, stormwater asset maps, survey and as-built information where available.
- Detailed study to review available data/model(s), Council information and the Council Flood Model and all relevant data and models. Include information of the existing situation as well as the future situation, after development of the area.
- Assess Flood Planning Level (FPL) and freeboard requirements in accordance with Council policy; and · Determine catchment hydrology.
- Recommendations to mitigate potential risks to overland flow and to meet the requested 1%AEP protection of the Oval.



Figure 1 - Norman Griffiths Oval - Six Maps



Figure 2 - Norman Griffiths Oval - Nearmap 14 July 2024







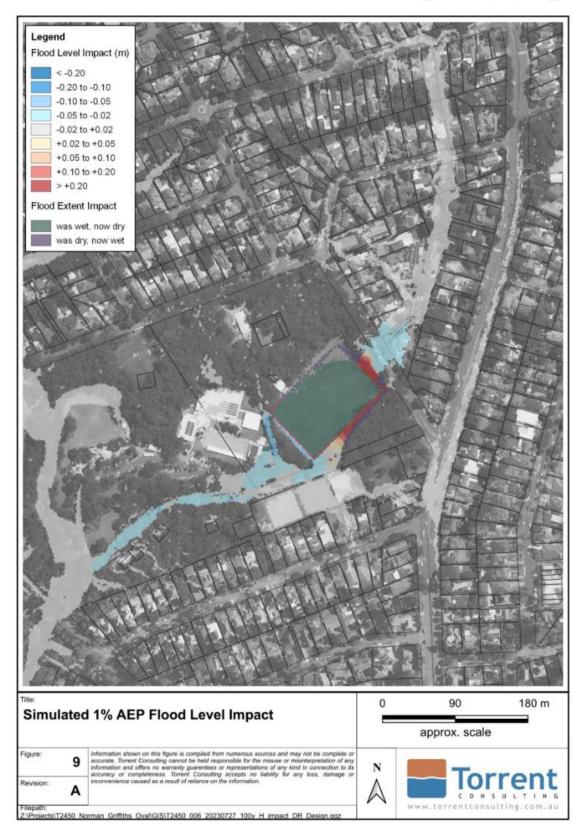


Figure 3 – 1% AEP Flood impact of the proposed oval works by Torrent



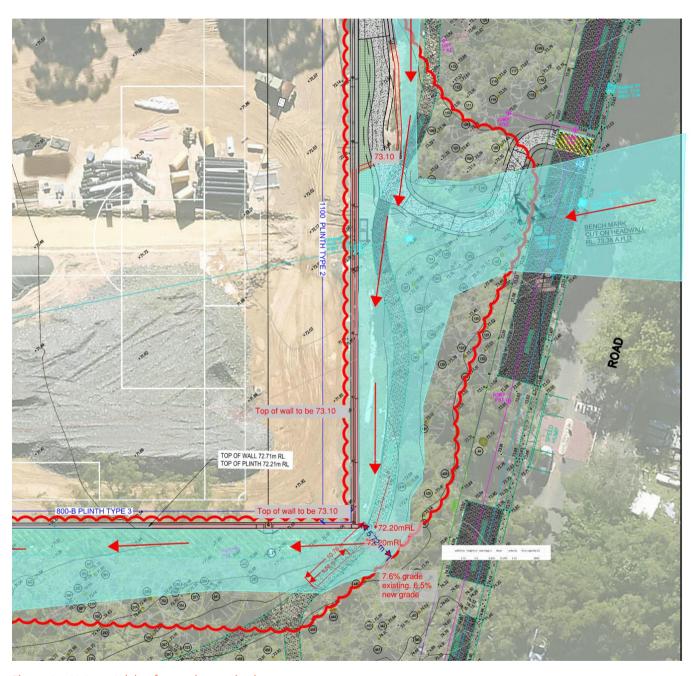


Figure 4 – 14 June Advice for works required

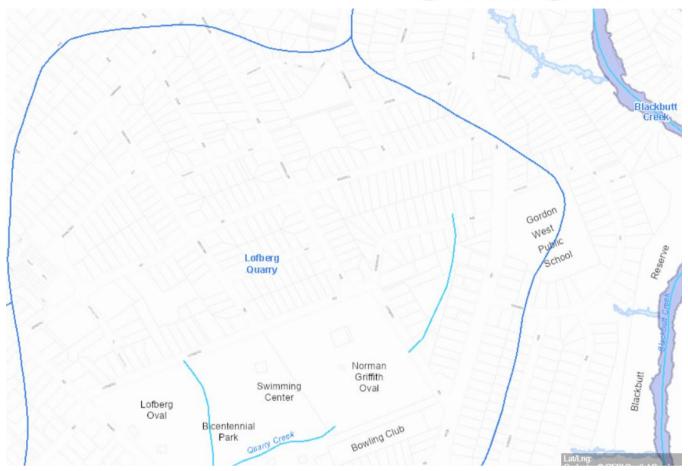


Figure 5 - Upstream Catchment, about 7cum/s total flow predicted for the 1% AEP event



2. Council request the documentation that assures the community that this sports field will work as a detention basin and is floodproof. This will require a review of the flood assessment and modelling of the entire system.

This documentation will give the community assurances that this design will work given the seriously concerning background we have highlighted in this letter.

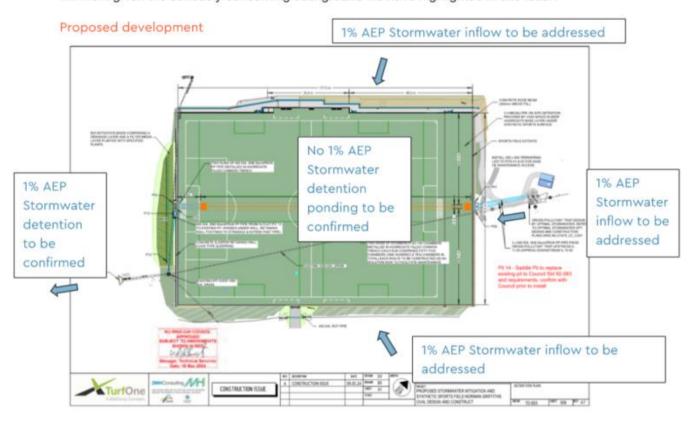


Figure 6 - Return brief to Council

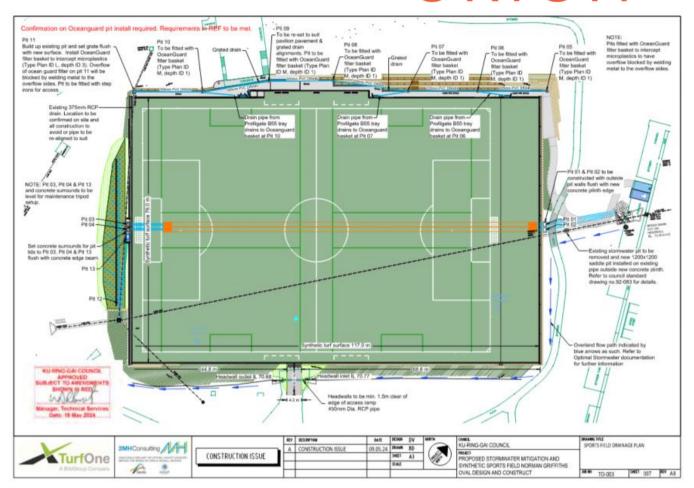


Figure 7 - Stamped Stormwater Drainage Plan



3. Preliminary Flood Impact Report

Orion have completed a preliminary flood impact review of the proposed redevelopment of Norman Griffiths Oval at 2 Lofberg Road, West Pymble.

We have received the following documentation for our review:

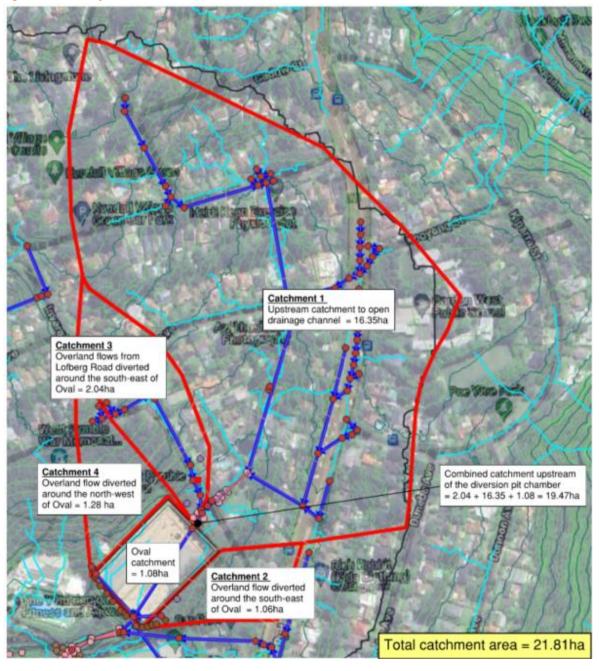
- Design drawings: "2024.05.17 IFC NORMAN GRIFFITHS SOCCER PITCH PLANS Approved Set" by 2MHConsulting (dated 9th May 2024)
- ii. Memo: "Overland Flow Path Assessment Feb 2024" by Optimal Stormwater (dated 18th Feb 2024)
- iii. Updated Memo: "Technical Memorandum Norman Griffith Oval Update 1.3.24" by Optimal Stormwater (dated 1st March 2024)
- iv. DRAINS Model
- v. TUFLOW Model (updated TUFLOW Model received 26/6/2024)

At this stage of the review, we provided our assessment of the TUFLOW model, DRAINS model and documentation to address compliance with the 1% AEP protection for the oval via the upstream wall, overland flow path capacity, adequate detention function and provide our recommendations for further design considerations.

1. Upstream Catchment Review

Upon preliminary assessment, it appears that the Oval is impacted by approximately 21.81 ha of contributing upstream catchment which ultimately drains into Quarry Creek. The upstream catchment can be roughly delineated into four main sub-catchments as shown in Figure 1 below. The primary contributing catchment comprises of approximately 16.35ha with a stormwater network connecting into a concrete-lined open channel at the upstream of Lofberg Road. Overland flows from 'Catchment 2' and 'Catchment 3' are conveyed around the south-west perimeter of the Oval, whilst 'Catchment 4' is diverted around the north-west side of the Oval before discharging into Quarry Creek.

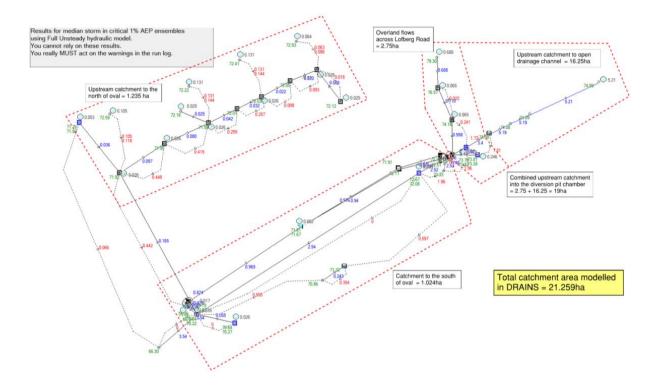
Figure 1. Preliminary Catchment Delineation



The total catchment area included in the DRAINS model received from Council is 21.259ha. As a catchment plan has not been provided, the individual sub-catchments cannot be verified, however from our understanding we have assumed the catchment breakdown shown in Figure 2 below.



Figure 2. Assumed Catchment Delineation



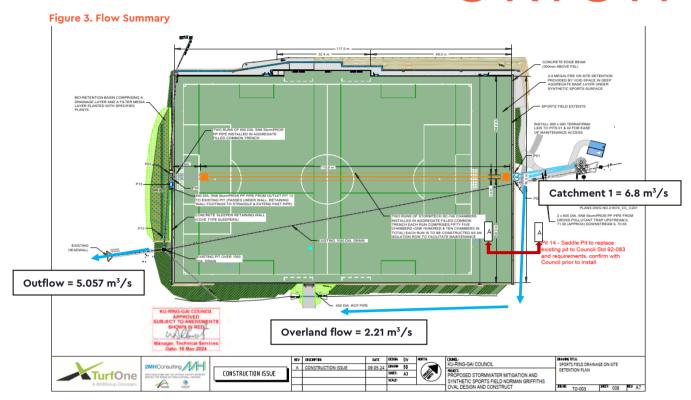
2. Preliminary DRAINS Analysis

At a high-level analysis of the upstream catchment, we have calculated these contributing catchments to Norman Griffiths Oval will produce roughly 6.8m³/s in the 1% AEP in the existing condition. The breakdown of contributing flows is shown in Figure 2 below. A summary of the design parameters made to the DRAINS model has been summarised in Appendix A.

Overland Flow Path Capacity

The overland flow path diverted around the eastern and southern perimeter of the oval requires 2.41m³/s of overland flow capacity without overtopping the proposed and partially constructed concrete plinth structure.





We note the required cross-sectional area of the overland flow path is 1.2m² at a slope of 0.5% and velocity of 1.84m/s to safely convey these flows. Please see the recommended options provided in the section below which allows for conveyance of the 2.21m³/s of overland flow.

3. Design Considerations & Recommendations

3.1. TUFLOW Model

Upon review of the TUFLOW model files, it appears the following are missing from the TUFLOW model package received from Council:

- 1d_xs cross section data
- 2d results files

The cross-section data defining the open drainage channel upstream of Lofberg Road has not been provided. There is potentially missing 1D/2D connectivity linking the upstream catchment conveyance through the channel. The dimensions of the drainage channel is required to be confirmed via the defined cross-section data.

We strongly recommend including the finished design surface of the oval and surrounding concrete plinth structures in the TUFLOW model. This will provide confirmation of the extents of overland flow paths and verify if the levels of the concrete plinth are sufficient to protect against overtopping onto the oval. This will confirm the impact of lifting the wall height as we do not want to create adverse flooding impacts upstream. No additional TUFLOW modelling was conducted at this stage.



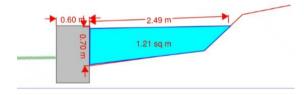
3.2. Stormwater Diversion Chamber

We have amended the weir arrangement in the pit diversion chamber to reflect the weirs built. We require confirmation of the cross-sectional area above the second weir structure to confirm flow capacity through the 1050dia pipe.

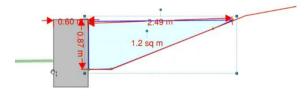
3.3. Final Recommendations

- The OSD has been designed with a capacity of 2.44 megalitres with an assumed void ratio of 40%. To confirm the OSD volume, we recommend the following to be completed: geotechnical testing and sampling of the proposed aggregate required to confirm the void ratio.
- We recommend providing a geofabric lining between the 50-150mm rock layer and finer aggregates to minimise the risk of settlement.
- We recommend the infiltration rate of the shockproof pad is confirmed by council.
- We recommend Council to confirm the decision on approach to achieve the overland flow capacity for the 2.21m³/s flowing on the eastern and southern boundaries of the oval, if the boundary wall is raised then the potential flood effect of the raised wall should be tested by modelling the raised wall in TUFLOW with the proposed wall structure.

Option 1:



Option 2:

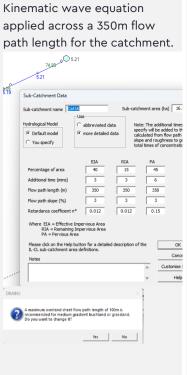


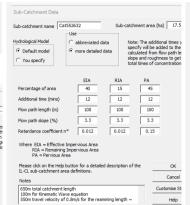
 Regardless of the wall solution, we recommend the proposed oval structures and stormwater system be modelled in TUFLOW to confirm the effect of the proposed development on upstream residential properties.

Appendix A

Item	Parameter	Existing Value from Council DRAINS Model	Updated Value 25/06/2024	Review Comments				
1	Catchment Analysis							
1.1	Catchment plan	Sub-catchment plan not provided.		Sub-catchment plan identifying delineated catchment areas modelled in DRAINS required for review.				
1.1	Upstream catchment	Total catchment modelled = 21.259ha Refer to Figure 2.	Total catchment delineated = 21.81ha Refer to Figure 1.	Confirm upstream catchment area includes all overland flows (refer to Figure 1 for catchment delineation)				
1.2	LIDAR/Survey		LIDAR from Elvis – 1m grid, 2020	Confirm LIDAR and survey data used for DRAINS and TUFLOW modelling is consistent.				
2.	Hydrology							
2.1	Initial Loss - Continuing Loss Model	Pervious Area Initial Loss = 27.4mm Pervious Area Continuing Loss = 1.8 mm/hr	Hydrology remains unchanged.	Note: ARR Data Hub recommends the continuing loss to be multiplied by the factor of 0.4. Losses have potentially been overestimated. Values from ARR Data Hub: Initial Loss = 33.0 mm Continuing Loss = 1.8 mm/hr Design summary to include justification of the values used. Sensitivity testing is also recommended to consider alternative hydrological models. Australian Rainfall & Runoff Dat Input Data Longitude 151.136 Latitude 33.764 Storm Losses Note: Burst Loss = Storm Loss - Preburst Note: These losses are only for rural use and are NOT FOR DIREC1 Note: As this point is in NSW the advice provided on losses and pre- the ARR Data Hub is to be considered, in NSW losses are derived o approaches depending on the available loss information. The contini the ARR Data Hub is to be multiplied by the factor of 0.4. ID Storm Initial Losses (mm) Storm Continuing Losses (mm/h)				

Kinematic wave 2.2 equation (Tc)





We note that this method of calculation is generally applicable to overland sheet flows in catchments with shallow slopes for flow paths up to 100m, and suitable for catchments with fairly uniform slope and roughness. The catchment comprises of approximately 3% slope and 60% impervious.

Kinematic wave equation for

- 650m total catchment length

the upstream 17.5ha

catchment:

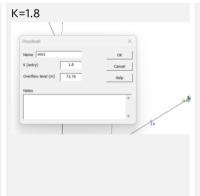
- 100m for Kinematic Wave equation
- 550m travel velocity of 0.8m/s for the remaining length ~ 12mins

Design summary to provide justification for the Tc calculations.

Hydraulic Structures

3.1 K factor at headwall (entrance loss coefficient)

3.

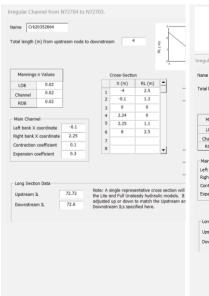


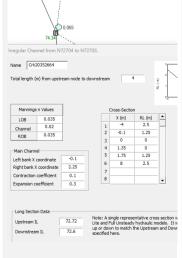
K=0.5

Entry loss coefficient adjusted to K=0.5 for the headwall located upstream of Lofberg Road. Representative of concrete headwalls with wingwalls at 10 to 25° (HEC-RAS manual, QUDM)

A higher entrance loss coefficient reduces the passage of flows through the pipe system and increases overland flows.

Open drainage 3.2 channel dimensions



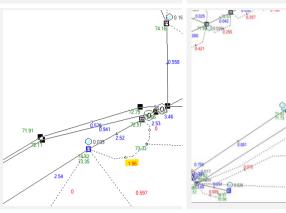


The Mannings value of the upstream channel has been applied as n=0.02 for the channel, LOB and ROB applied across the 12m width of the defined flow area.

Overbanks updated to a higher Mannings value to represent the vegetation adjacent to the length of the channel, n=0.035 for light brush on banks (Chow, 1959)

The channel structure was measured to be 1.30m base width, 1.75m top width, 1.25m depth from site visit. Variations in the cross section of the channel to be confirmed in the

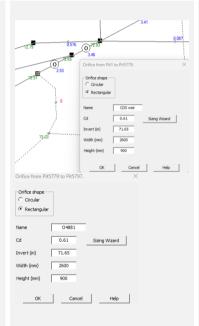
3.2 Connectivity of overflow route



cross-section data modelled in TUFLOW.

Overflow route to be connected to the downstream pit to ensure the 2.21m³/s is conveyed as overland flow. In the DRAINS modelled received from Council, the overflow route is modelled to enter Pit2, however should instead be diverted to the downstream node.

3.4 Diversion chamber / weir configuration

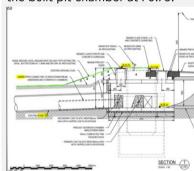




70.75

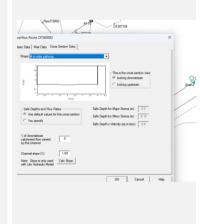
2600

We have amended the weirs in the DRAINS model to reflect a 900mm high weir with the invert level set at the invert of the built pit chamber at 70.75.



3.4 Overland Flow Paths



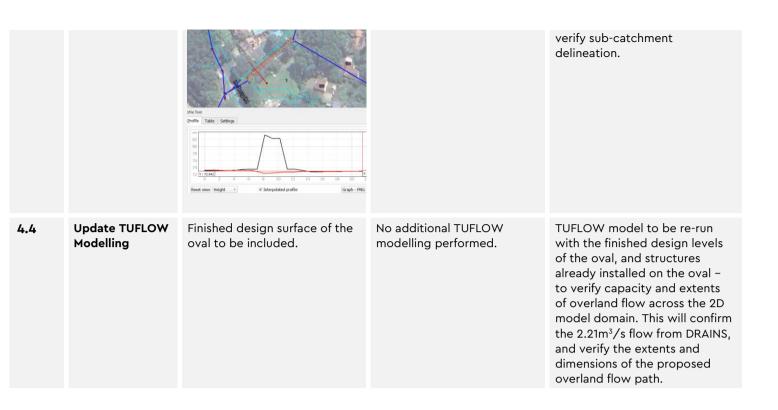


Overland flow path to be updated in DRAINS to reflect a narrower cross section through the bushland area, with the concrete plinth level of FL72.11 added to reflect flow diversion around the oval.

4m wide flow path does not reflect existing conditions. Noting the extent of the overland flow path is limited by ecologically protected bushland.

This is also required to be modelled in TUFLOW to accurately represent overland flow extents and depth across the 2D domain.

3.5	Overland Flow Paths	P33,047Ppv6377 OF50002 OF500		Overland flow path to be revised.
3.6	OSD Volume	Volume modelled = 2421.83m3 ■ Easin2 Volume File Edit Properties Comparison		Volume in the system reflects the design 2.4 megalitres. Geotechnical testing required to confirm the 40% void ratio as specified in the design drawings.
,	TUFLOW Model			
4.				
4.1	Catchment delineation	2d_code and catchment boundary data provided, however sub-catchment delineation GIS files not provided.	No additional TUFLOW modelling performed.	Sub-catchment delineation for the TUFLOW model to be provided for review and comparison against the catchments modelled in DRAINS.
4.2	1d_xs cross section database	Id_xs data not provided, missing connectivity between open drainage channel and downstream pipes.	No additional TUFLOW modelling performed.	1d_xs database and 1d_xs.csv files e.g. "USC_000.csv" to be provided to verify the defined cross-sectional areas and confirm whether missing 1D/2D link conveyance of upstream catchment conveyance via drainage channel. TUFLOW model with the 1D links to be provided.
4.3	Terrain data	A profile section was taken across the drainage channel from the NGO_Base_ARR1987_100y_60 m.2dm output file which shows an unusually high elevation throughout the channel.	No additional TUFLOW modelling performed.	The base topography data was not provided, the .2dm elevation output file was used to roughly check for any 2d anomalies modelled. The .2dm file was checked against (1m grid LIDAR data 2020) All topography source data (LIDAR, survey, design TINs) to be provided for review and to



4. Detailed Flood Impact Analysis

Orion has provided an independent analysis to allow sign-off of the Normal Griffiths oval works in terms of its flood protection level, and the compliance of the on-site stormwater detention volume provided in the design and that constructed by close analysis of the Tuflow model and drains models as recommended in stage 1 and close analysis of the as built site records.

This stage of works has provided the analysis required for an independent sign-off as to the level of flood protection specified by council, as well as the performance of the oval on site detention system and storage method in the void space of a gap graded gravel layer in accordance with the design plans stamped and approved by Council.

AS part of these works we have provided the following

- Detailed study to review available data/model(s), Council information and the Council Flood Model and all relevant data and models. Include information of the existing situation as well as the future situation, after development of the area.
- Assess Flood Planning Level (FPL) and freeboard requirements in accordance with Council policy; and · Determine catchment hydrology.
- Recommendations for amendments and option for the stamped approved design to mitigate potential risks to overland flow and to meet the requested 1%AEP protection of the Oval and the performance of the detention storage.

5. Reference Documents

In preparation for this Flood Impact Advice, the following documents were referred to:

- Contractor drains model
- Torrent high level flood impact
- Council Brief for Outcome required
- Stamped approved civil plans
- Six Maps
- Nearmap

6. Modified Path design to accommodate overland flow

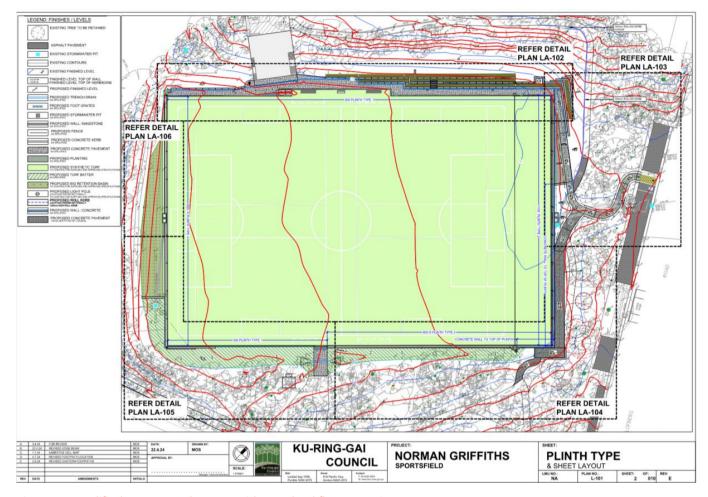


Figure 8 - Modified eastern paths to provide overland flow capacity



Figure 9 - Modified eastern paths to provide overland flow capacity

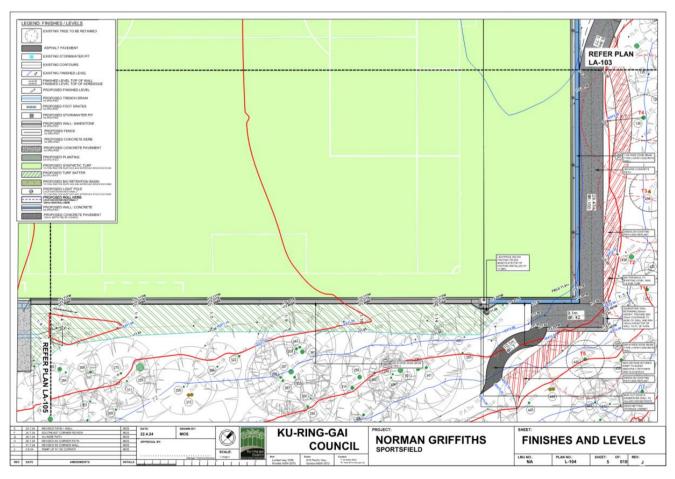


Figure 10 - Modified eastern paths to provide overland flow capacity

7. Flood Impacts

There is predicted flooding on and adjacent the site in the proposed condition

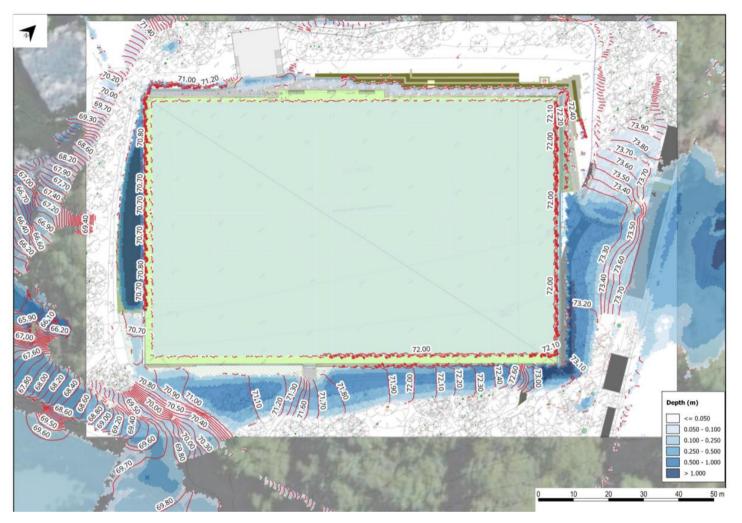


Figure 11 - Design Flood levels (1% AEP) extent with proposed oval and the agreed upstream diversion works in place

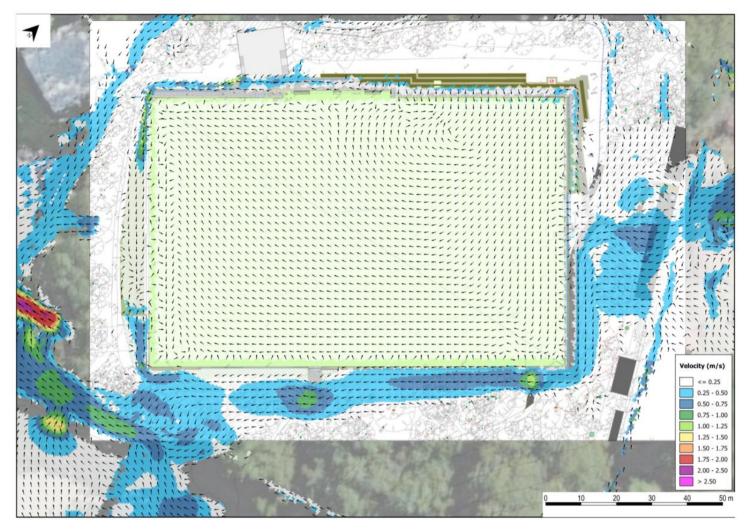


Figure 12 – Design Flood (1% AEP) velocities with proposed oval and the agreed upstream diversion works in place

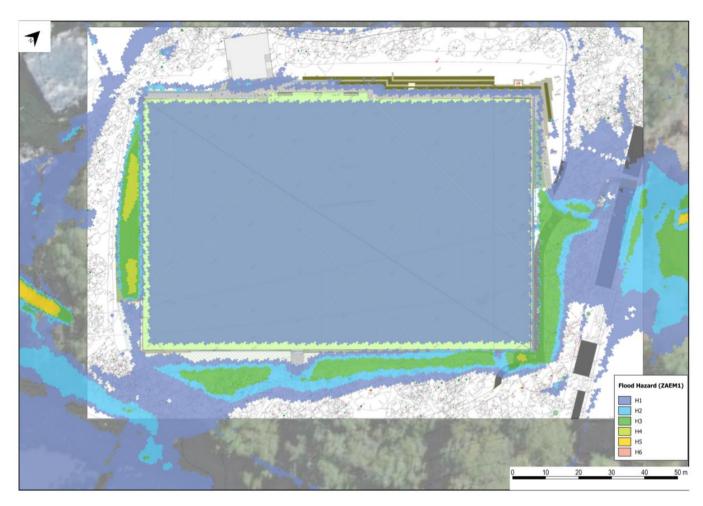


Figure 13 – Design Flood (1% AEP) Hazard with proposed oval and the agreed upstream diversion works in place

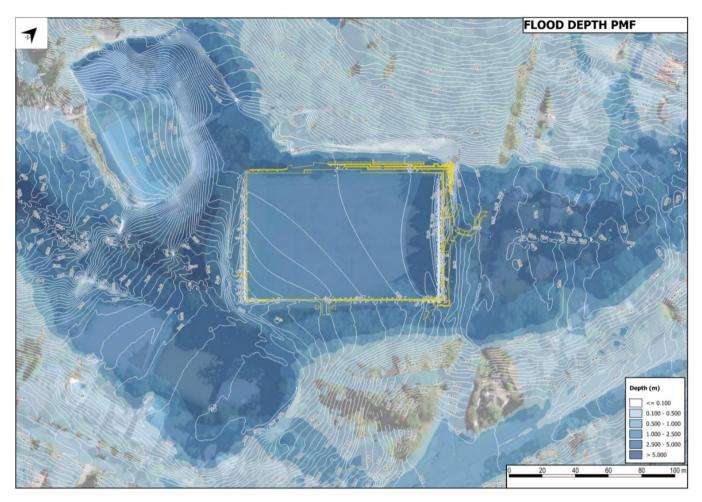


Figure 14 -Flood levels (PMF) extent with proposed oval and the agreed upstream diversion works in place

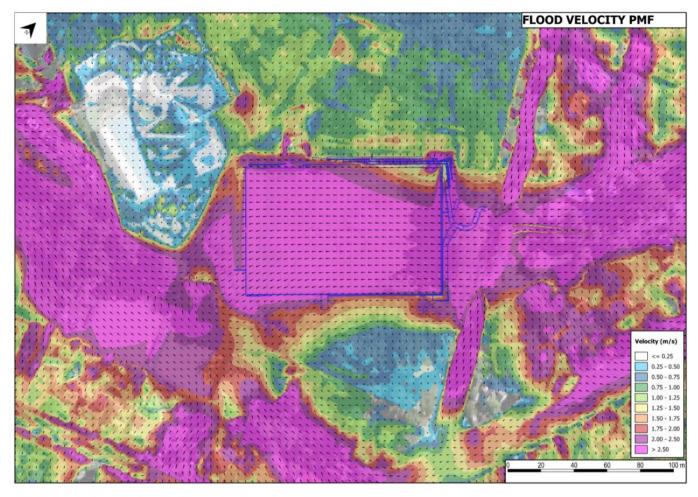


Figure 15 - Velocity (PMF) extent with proposed oval and the agreed upstream diversion works in place

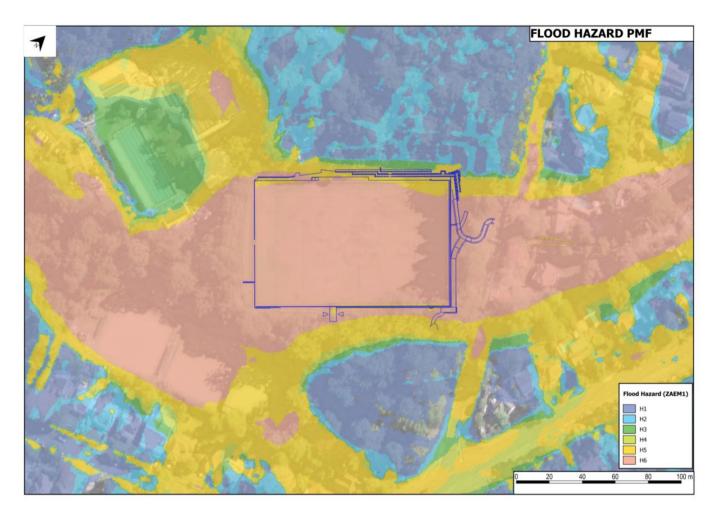


Figure 16 – Hazard for Probable Maximum Flood with proposed oval and the agreed upstream diversion works in place

8. Recommendations for Norman Griffiths Oval

We are happy to sign off on the diversion of the overland flow flood risk in the 1% AEP storm event from the upstream catchment east of Lofberg Road Quarry creek around the oval site, provided

- 4. the 3m wide concrete pathway specified at the levels specified is constructed in accordance with our markups to ensure sufficient capacity is provided for the overflow occurring in this flood event.
- 5. The diversion wall is constructed to the top of wall levels we have specified
- 6. The drainage at the base of the bleachers is installed and maintained
- 7. Our concerns with the settlement risk of the field drainage media are addressed by the addition of a bidim later between the detention storage rockfill and the bedding layer for the shockpad and playing surface to limit settlement of the playing surface via material loss from the bedding layer into the detention storage layer.

We receive confirmation from a geotechnical engineer on the void ratio for the detention storage rockfill (40% specified)

Yours sincerely,

Orion Group | Stephen Brain - Technical Director

Appendix A - stamped oval drawings

NORMAN GRIFFITHS OVAL, 2 LOFBERG RD, WEST PYMBLE NSW 2073. SYNTHETIC FOOTBALL (SOCCER) PITCH REDEVELOPMENT

NOTE: PLANS TO BE READ IN CONJUNCTION WITH KU-RING-GAI COUNCIL FINISHES & LEVELS PLAN PLAN NO. L-103.





DEVELOPMENT SITE LOCALITY

CIVIL DRAWINGS LIST:

- 001 COVER PAGE
- 002 GENERAL NOTES
- 003 SITE MANAGEMENT & EROSION & SEDIMENT CONTROL PLAN
- 004 DEMOLITION PLAN
- 005 SYNTHETIC SPORTS FIELD FINISHES AND SURFACES PLAN
- 006 SPORTS FIELD FOOTPATH & SECTION DETAIL PLAN
- 007 SPORTS FIELD DRAINAGE PLAN
- 008 SPORTS FIELD ON-SITE DETENTION PLAN
- 009 STORMWATER LONG SECTIONS & PIT SCHEDULES
- 010 STORMWATER LONG SECTIONS
- 011 SPORTS FIELD INLET PITS DETAILS
- 012 SPORTS FIELD OUTLET PITS DETAILS
- 013 ON-SITE DETENTION ISOMETRIC LAYOUT

- 014 ON-SITE DETENTION PROFILE SECTION
- 015 ON-SITE DETENTION CALCULATIONS & SECTIONAL VIEWS
- 016 BIO-RETENTION BASIN LAYOUT
- 017 BIO-RETENTION SECTION DETAIL & PLANTING SCHEDULE
- 018 SPORTS FIELD SECTION DETAILS SHEET 1
- 019 SPORTS FIELD SECTION DETAILS SHEET 2
- 020 SPORTS FIELD SECTION DETAILS SHEET 3
- 021 SPORTS FIELD SECTION DETAILS SHEET 4
- 022 SPORTS FIELD SECTION DETAILS SHEET 5
- 023 SPORTS FIELD SECTION DETAILS SHEET 6
- 024 SPORTS FIELD FENCE DETAILS
- 025 SPORT FIELD EMERGENCY/MAINTENANCE ACCESS
- 026 SPORT FIELD SETOUT PLAN

- 027 PATH CHAINAGES & SAW CUT PLAN
- 028 PATH LONGITUDINAL SECTION
- 029 PATH CROSS SECTION SHEET 1
- 030 PATH CROSS SECTION SHEET 2
- 031 PATH CROSS SECTION SHEET 3
- 032 PATH CROSS SECTION SHEET 4
- 033 RETAINING WALL LONG SECTION & CHAINAGES
- 034 RETAINING WALL DETAILS
- 035 WEST GATE AND LOW FENCE DETAIL
- 036 NORTH ACCESS GATE & SOUTH ACCESS GATE DETAIL
- 037 SOUTH NETTING CABINET DETAIL
- 038 NORTH NETTING CABINET DETAIL





CONSTRUCTION ISSUE

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KU-RING-GAI COUNCIL
DDG IEST

PROJECT:
PROPOSED STORMWATER MITIGATION AND
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS
OVAL DESIGN AND CONSTRUCT

COVER PAGE

TO-003

HS JOB NO:

SHEET: 001

GENERAL NOTES

- DRAWINGS ARE TO BE READ IN CONJUNCTION WITH ALL OTHER PROJECT DRAWINGS.
- ALL WORKS TO BE CARRIED OUT IN ACCORDANCE WITH CIVIL SPECIFICATION, APPROVED PLANS AND TO THE SATISFACTION OF THE
- SURVEY BACKGROUND INFORMATION SUPPLIED BY OTHERS.
- EXISTING CONTOURS SHOWN REFLECT SITE CONDITIONS AT TIME OF SURVEY.
- ALL DIMENSIONS SHOWN ARE IN MILLIMETERS UNLESS NOTED OTHERWISE.
- LEVELS ARE TO AUSTRALIAN HEIGHT DATUM.
- ALL DIMENSIONS RELEVANT TO SETTING OUT SHALL BE CONFIRMED AND VERIFIED BY THE CONTRACTOR BEFORE CONSTRUCTION IS COMMENCED. THE CONTRACTOR SHALL REPORT ANY DISCREPANCIES TO THE SUPERINTENDENT.
- 2MH DOES NOT ACCEPT ANY RESPONSIBILITY FOR THE ACCURACY, ADEQUACY OR APPROPRIATENESS OF THE SPORTSFIELD DESIGN, GEOTECHNICAL WORKS OR PAVEMENT DESIGN.

STANDARD EXISTING SERVICES NOTES

- 2MH ACCEPT NO RESPONSIBILITIES IN RELATION TO EXTENT AND LOCATION OF EXISTING SERVICES IN THE VICINITY OF THE SITE.
- CONTRACTORS MUST ASCERTAIN THE PRECISE LOCATION AND DEPTH OF ALL EXISTING SERVICES WHICH COULD BE AFFECTED BY THE WORKS WHERE EXISTING SERVICES ARE FOUND TO BE IN CLASH OF THE WORKS THE CONTRACTOR SHOULD NOTIFY THE SUPERINTENDENT ACCORDINGLY.
- THE CONTRACTOR SHALL LIAISE WITH ALL RELEVANT SERVICE AUTHORITIES WITH RESPECT TO ANY SERVICE ALTERATIONS OR FOR WORKS IN VICINITY OR CLOSE PROXIMITY TO EXISTING SERVICES, THE CONTRACTOR SHALL BE REQUIRED TO SEEK CLEARANCE, PROGRAM AND COORDINATE THESE WORKS WITH THE RELEVANT SERVICE AUTHORITY AND THEIR CONTRACTORS
- ALL SERVICE CONDUITS TRENCHES UNDER PAVEMENTS ARE TO BE BACKFILLED WITH 20mm 3% CEMENT TREATED CLASS 3 CRUSHED ROCK COMPACTED TO A DENSITY NOT LESS THAN 95% OF THE MAXIMUM DRY DENSITY VALUE DETERMINED BY THE MODIFIED COMPACTION TEST IN ACCORDANCE WITH A.S.1289.5.2.1-2003.
- ALL TABLE DRAINS AND VERGES ARE TO BE REINSTATED UPON COMPLETION OF WORKS TO THE SATISFACTION OF THE RELEVANT AUTHORITY
- CONTRACTOR TO IMPLEMENT SEDIMENT CONTROL BARRIERS/METHODS TO ENSURE SEDIMENT TRANSFER TO DOWNSTREAM DRAINS/SURFACES FROM SITE DOES NOT OCCUR. SHOULD TRANSFER OF SEDIMENT OCCUR IT IS THE CONTRACTORS RESPONSIBILITY TO REMOVE AND MAKE GOOD ALL DISTURBED AREAS AT THE DISCRETION OF THE SUPERINTENDENT.
- ALL TRENCHING WORKS TO BE IN ACCORDANCE WITH THE RELEVANT ACT AND REGULATIONS.
- ALL EXISTING ASSETS AFFECTED BY THE WORKS: EG SIGNS, VEHICLE CROSSINGS, FOOTPATHS, KERB AND LINEMARKING SHALL BE REINSTATED BY THE CONTRACTOR PRIOR TO THE COMPLETION OF THE WORKS TO THE SATISFACTION OF THE SUPERINTENDENT/OR THEIR REPRESENTATIVE.

STANDARD EARTHWORKS NOTES

- LEVELS PROVIDED ARE FINISHED SURFACE LEVELS. EARTHWORKS SHOULD THEREFORE BE FINISHED AT THE APPROPRIATE LEVELS TO ALLOW FOR THE CONSTRUCTION OF PAVEMENTS AND SHOULDERS AS DOCUMENTED.
- EARTHWORK SPOIL IN EXCESS OF SITE FILL REQUIREMENTS SHALL BE DISPOSED OFF SITE AT CONTRACTORS EXPENSE OR SPREAD ONSITE AT THE DIRECTION OF COUNCIL'S PROJECT MANAGER.
- EXCAVATED MATERIAL WHICH CONFORMS WITH THE SPECIFICATION REQUIREMENTS FOR FILL MAY BE USED AS BACKFILL
- DURING CONSTRUCTION THE CONTRACTOR SHALL BE RESPONSIBLE FOR CONSTRUCTING AND MAINTAINING A TEMPORARY SITE DRAINAGE SYSTEM AND TO MAINTAIN THE SITE IN A DRY AND STABLE CONDITION. DETAILS OF THE DRAINAGE SYSTEM SHALL BE SUBMITTED FOR THE APPROVAL OF THE SUPERINTENDENT.
- ALL COMPACTION TO BE CARRIED OUT IN ACCORDANCE WITH COMPACTION PROCEDURES AS DEFINED IN AS-1289 5.2.1 TEST PROCEDURE, CERTIFICATION IS TO BE AN INDEPENDENT GEOTECHNICAL ENGINEER (AT CONTRACTORS EXPENSE).
- FILL AREAS TO BE CLEARED AND STRIPPED OF ALL ORGANIC MATERIAL AND TOPSOIL PRIOR TO PLACEMENT OF SELECTED FILL MATERIAL. FILL AREAS ARE TO BE INSPECTED BY THE SUPERVISING ENGINEER PRIOR TO ANY FILL BEING PLACED. FILL IS TO BE PLACED AND COMPACTED IN LAYERS, WITH A MINIMUM COMPACTION OF 98% OF THE MAXIMUM DRY DENSITY AS DETERMINED BY THE STANDARD COMPACTION TEST BEING ACHIEVED.
- ALL STRIPPED TOPSOIL/SILT MATERIAL SHALL BE STOCKPILED ON SITE IN AREA AS DIRECTED BY THE SUPERINTENDENT.
- BATTERS ARE TO BE TOPSOILED & SEEDED TO A DEPTH OF APPROXIMATELY 150mm USING MATERIAL STOCKPILED FROM STRIPPING FOR BOTTOM 100mm AND APPROVED IMPORTED SANDY LOAM FOR A TOP 50mm.

STANDARD PAVEMENTS, KERBING AND ANCILLARY WORKS

- WHERE NEW ASPHALT, CONCRETE K & C, PATHS AND DRIVEWAYS MATCH INTO EXISTING, THE EXISTING SURFACE IS TO BE SAW CUT AND MATCHED NEATLY.
- PAVEMENT DEPTH SPECIFIED IS A MINIMUM DEPTH AND MAY BE VARIED BY THE SUPERINTENDENT/OR THEIR REPRESENTATIVE. SOFT SPOTS SHALL BE EXCAVATED TO A PROOF ROLLED BASE AND BACKFILLED WITH APPROVED MATERIAL COMPACTED IN 200mm LAYERS TO ACHIEVE TO A DENSITY NOT LESS THAN 98% OF THE MAXIMUM DRY DENSITY VALUE DETERMINED BY THE STANDARD COMPACTION TEST IN ACCORDANCE WITH A.S.1289.5.1.1-2003.
- AGRICULTURAL DRAINS ARE TO BE PLACED BEHIND ALL KERB AND CHANNEL, KERB ONLY AND EDGE STRIPS IN ACCORDANCE WITH STANDARD DRAWINGS.
- SET OUT DIMENSIONS GIVEN TO KERBING ARE TO THE INVERT OF KERB UNI ESS SPECIFIED OTHERWISE.

STANDARD DRAINAGE AND PLUMBING WORKS:

- ALL GROUND SURROUNDING THE STRUCTURE SHALL BE GRADED AWAY AT MINIMUM 1 in 20 FOR AT LEAST 1.0m, UNLESS NOTED OTHERWISE.
- WATER RUN-OFF SHALL BE COLLECTED AND CHANNELED AWAY FROM THE FOOTINGS DURING CONSTRUCTION. 2.
- A 100mm DIA. SUB-SOIL DRAINS LAID AT A MINIMUM GRADE OF 1 in 100 AT THE HIGH END SIDES OF THE STRUCTURE BELOW THE CRUSHED ROCK BASE LAYER. AG DRAIN TO BE LAID ON BEDDING SAND AND SURROUNDING WITH "ONE SIZED" AGGREGATE COVERED WITH GEO TEXTILE. CONNECT AG DRAIN INTO NEW STORM WATER SYSTEM VIA 400x400 GRATED JUNCTION OR UNLESS NOTED OTHERWISE AND DISCHARGE TO THE LEGAL POINT OF DISCHARGE.
- 4. PIT COVER LEVELS TO MATCH SURROUNDING FINISHED LEVELS.

STANDARD CONCRETE NOTES

- NO CONCRETE SHALL BE MIXED OR PLACED, WITHOUT THE APPROVAL OF THE SUPERINTENDENT, WHILE THE AIR TEMPERATURE IS, OR LIKELY TO BE WITHIN 24 HOURS, BELOW 5 DEGREES CELSIUS OR WHILE THE SHADE TEMPERATURE EXCEEDS 38 DEGREES CELSIUS. ALL CONCRETE SHALL BE PLACED IN THE DRY. PRIOR TO PLACING CONCRETE THE AREA SHALL BE CLEAN AND MOIST BUT FREE FROM ANY WATER PONDING.
- THE CONCRETE SHALL BE MIXED IN THE QUANTITIES REQUIRED FOR IMMEDIATE USE AND SHALL BE PLACED IN POSITION AS RAPIDLY AS POSSIBLE. ANY CONCRETE WHICH HAS DEVELOPED INITIAL SET, OR WHICH DOES NOT REACH THE FORMS WITHIN 30 MINUTES AFTER THE WATER HAS BEEN ADDED (EXCEPT WHEN TRANSPORTED IN AGITATOR TRUCKS) SHALL NOT BE USED.
- THE CONCRETE SHALL BE DEPOSITED IN THE FORMS, WITHOUT SEPARATION OF THE AGGREGATES. CONCRETE SHALL NOT BE DROPPED FREELY FROM A HEIGHT GREATER THAN 1.2m OR BE DEPOSITED IN LARGE QUANTITIES AT ANY POINT AND MOVED OR WORKED ALONG THE FORMS. CONVEYING EQUIPMENT, INCLUDING OPEN TROUGHS AND CHUTES, WHERE USED, SHALL BE MADE OF METAL OR HAVE METAL LININGS. WHERE USED ON STEEP SLOPES, TROUGHS AND CHUTES SHALL BE EQUIPPED WITH BAFFLES, OR BE PLACED IN SHORT LENGTHS IN SUCH A WAY THAT THE DIRECTION OF FLOW OF THE CONCRETE IS CHANGED. THE CONCRETE SHALL BE PLACED IN HORIZONTAL LAYERS IN ONE CONTINUOUS OPERATION BETWEEN THE ENDS OF THE WORKS AND/OR CONSTRUCTION JOINTS.CARE SHALL BE TAKEN TO FILL EVERY PART OF THE FORMS AND TO WORK THE COARSER AGGREGATE BACK FROM THE FACE. THE FRESHLY PLACED CONCRETE SHALL BE COMPACTED BY CONTINUOUS SPADING SLICING OR BY VIBRATOR UNITS. VIBRATORS SHALL NOT BE LEFT IN ONE POSITION FOR MORE THAN 30 SECONDS, AND SHALL NOT BE PERMITTED TO REST ON REINFORCEMENT.
- ALL EXPOSED SURFACES OF THE FRESHLY PLACED CONCRETE SHALL BE KEPT MOIST EITHER BY USE OF PLASTIC SHEETING, DAMP SAND OR COMMERCIAL CURING COMPOUNDS, IN ACCORDANCE WITH AS3799, FOR A MINIMUM PERIOD OF 3 DAYS. DURING THIS TIME THE WORKS MUST BE ADEQUATELY PROTECTED FROM THE EFFECTS OF EXCESSIVE SURFACE EVAPORATION, RAIN, RUNNING WATER, VANDALISM AND OTHER CAUSES LIKELY TO DAMAGE THE CONCRETE, ALL COSTS INVOLVED IN MAKING GOOD OR REPLACING ANY WORK THAT HAS BEEN DAMAGED DUE TO THE ABOVE MENTIONED FACTORS SHALL BE BORNE BY THE CONTRACTOR.
- CURING FOR CONCRETE SHALL GENERALLY BE IN ACCORDANCE WITH THE APPROPRIATE SURFACE EXPOSURE CLASSIFICATION IN AS







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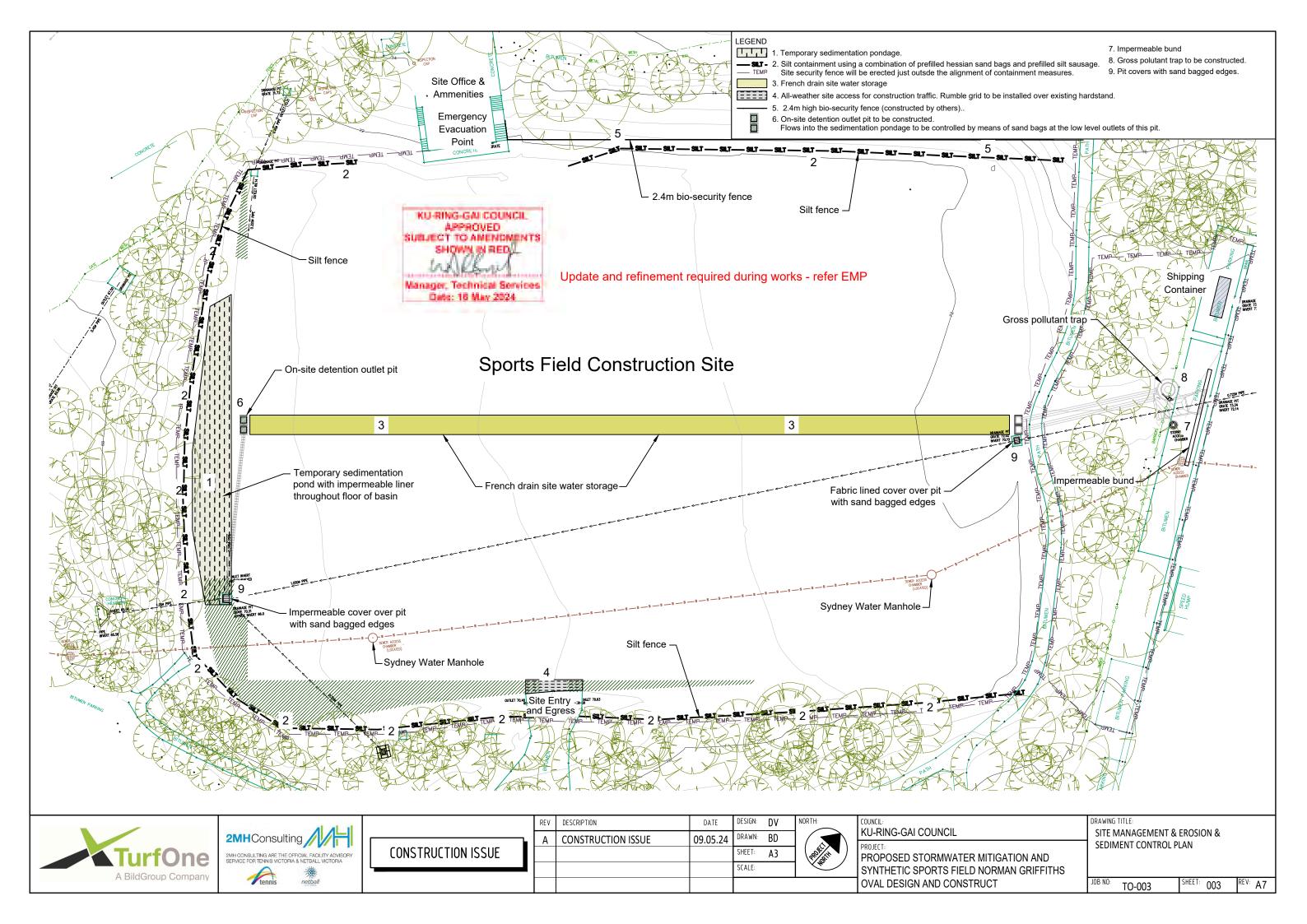
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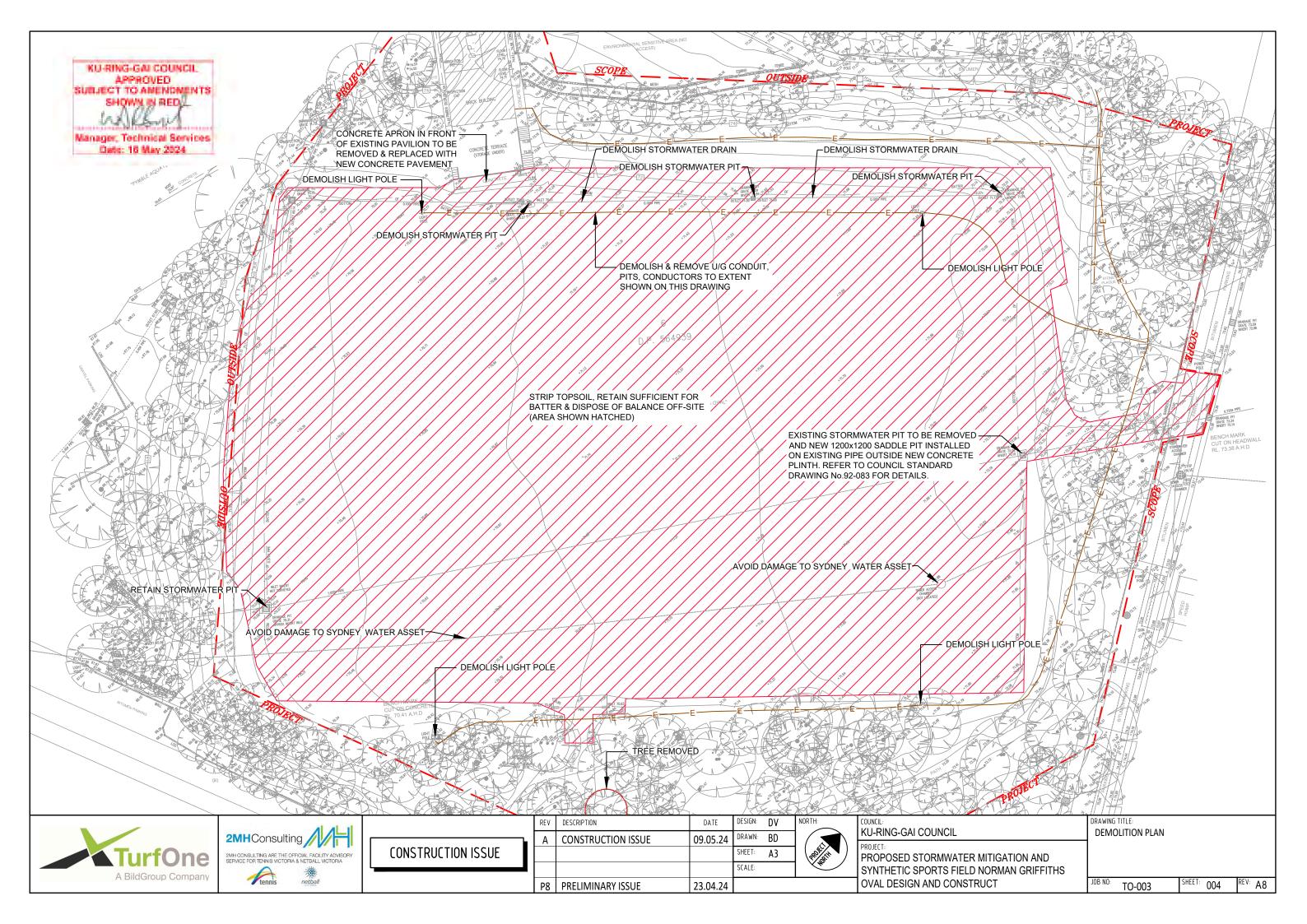
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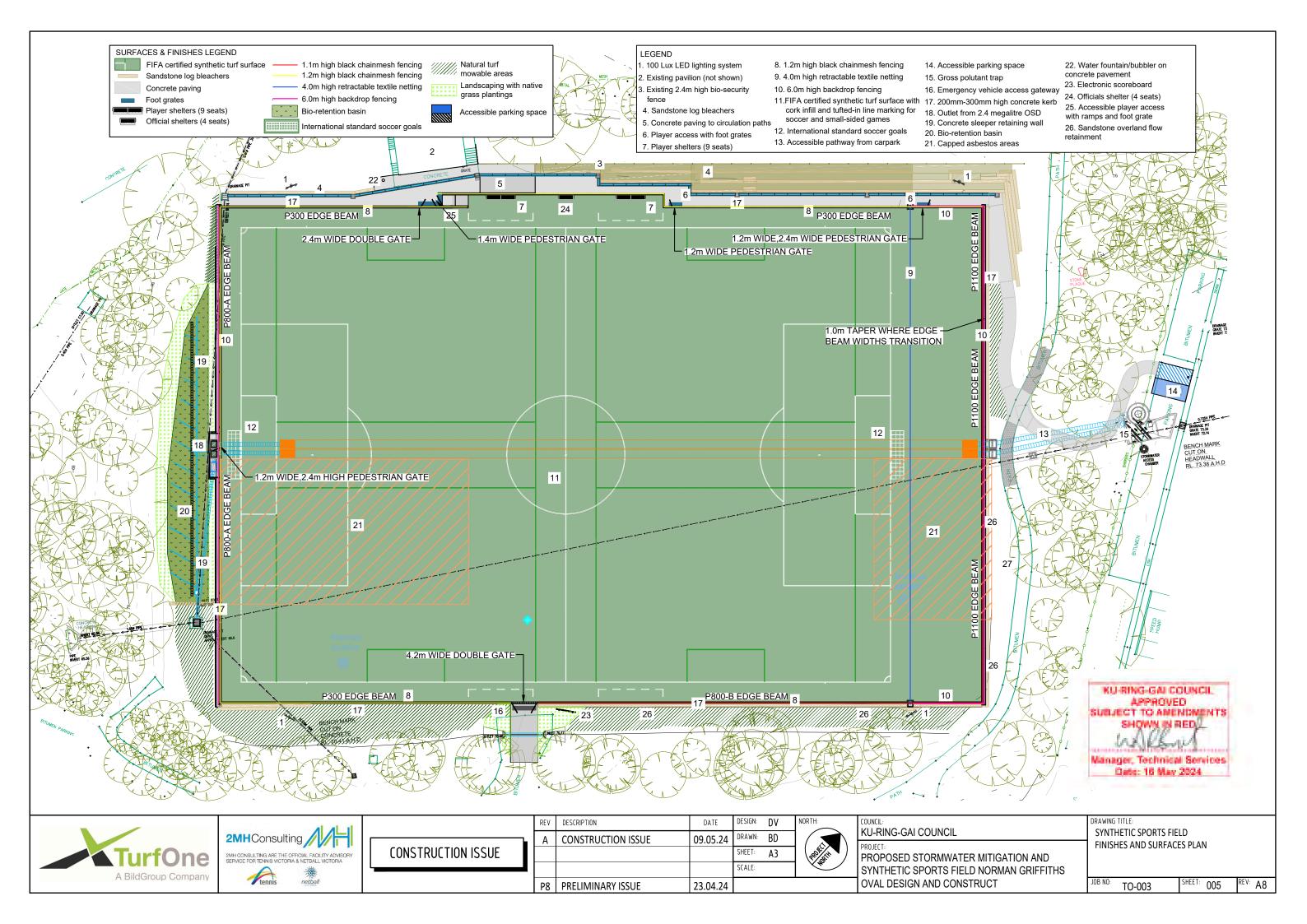
PROPOSED STORMWATER MITIGATION AND SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS OVAL DESIGN AND CONSTRUCT

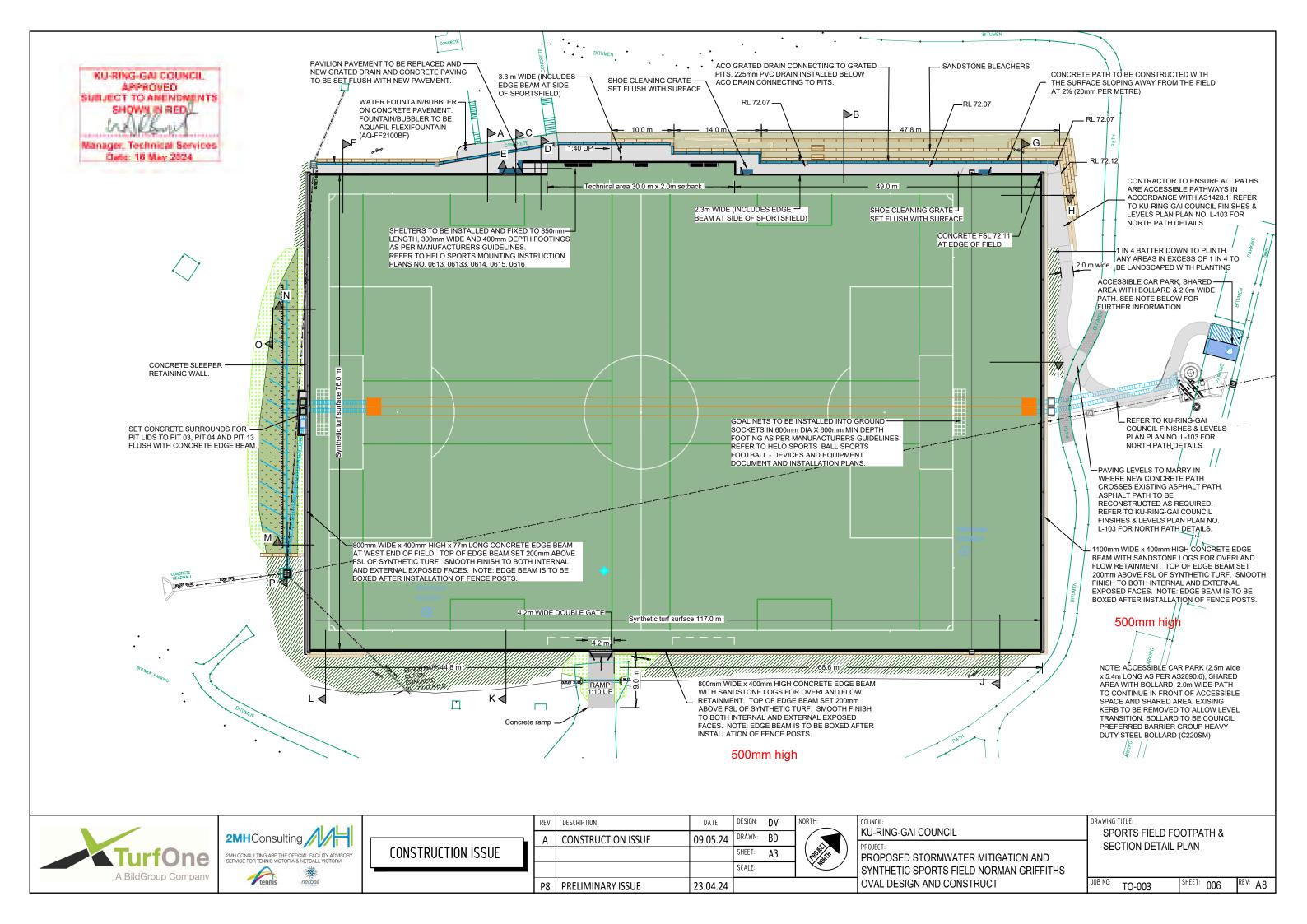
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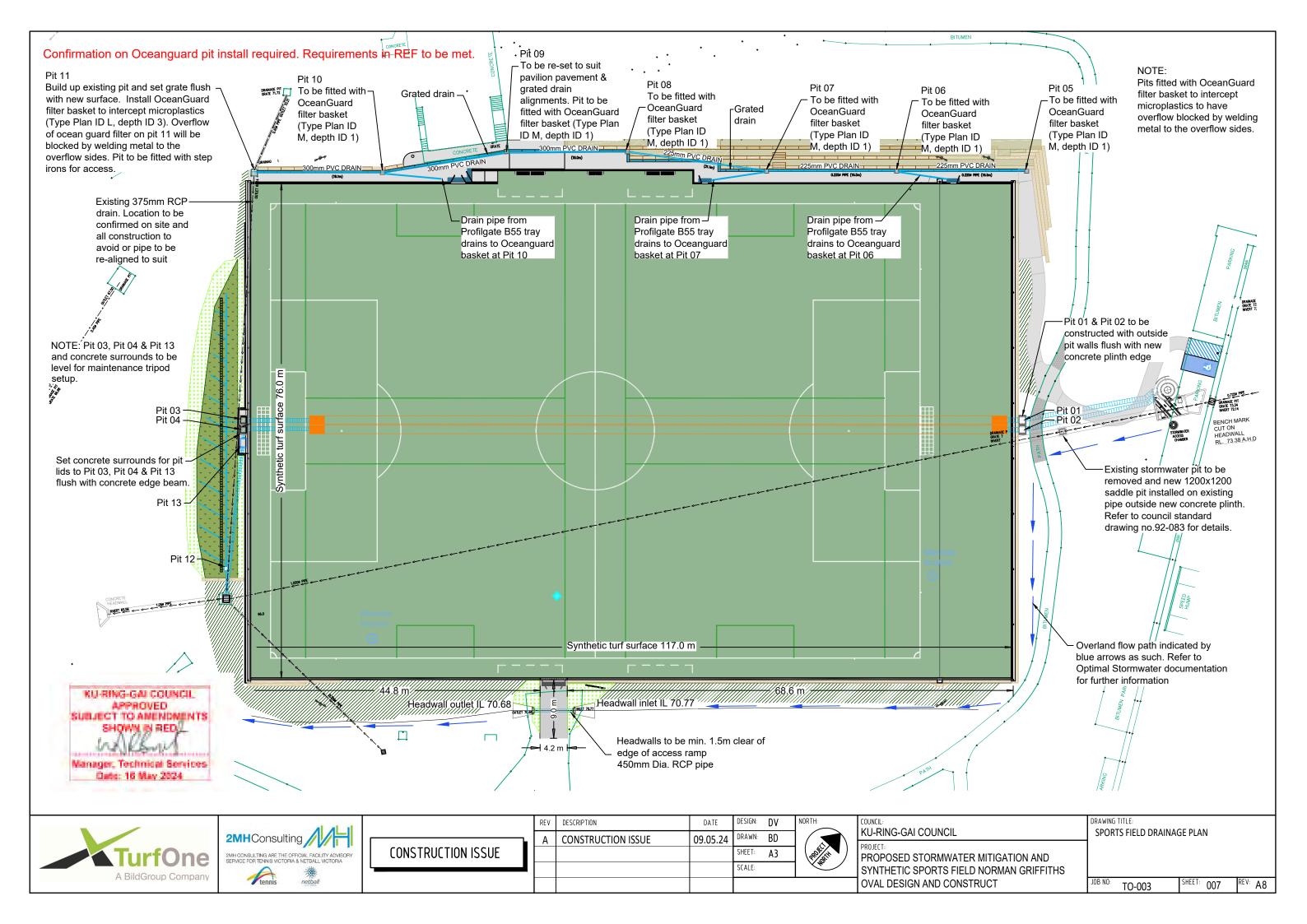
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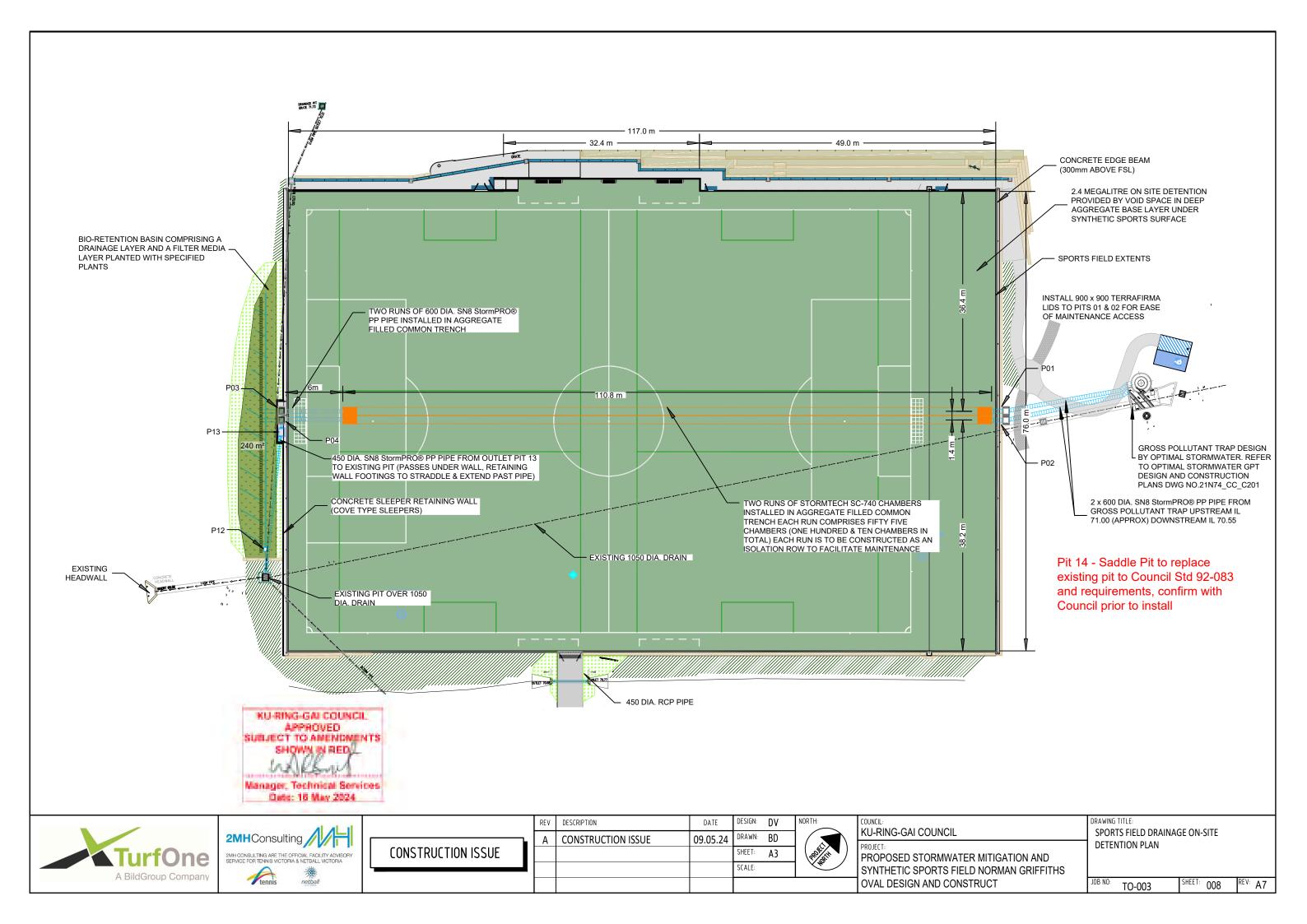


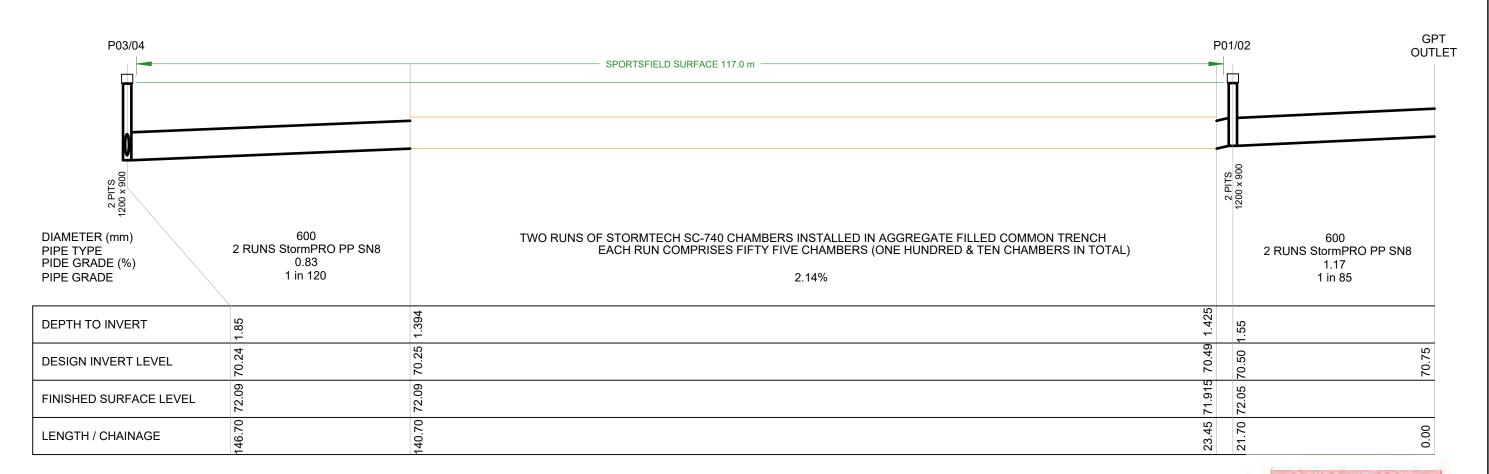


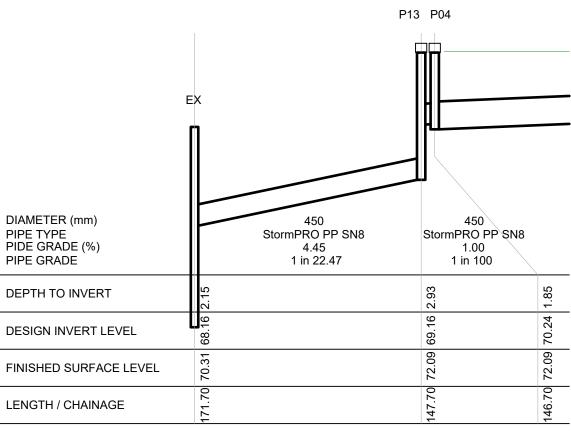












Pit 14 - Saddle Pit to replace existing pit to Council Std 92-083 and requirements, confirm with Council prior to install KU-RING-GAI COUNCIL APPROVED SUBJECT TO AMENDMENTS SHOWN IN RED

Manager, Technical Services Date: 16 May 2024

PIT	PIT TYPE	LENGTH	WIDTH	DEPTH	INLETO	UTLET	INVERT RL	COVER RL	EASTING	NORTHING	COVER	CLASS
01	JUNCTION PIT INLET	1200	900	1550	600	600	70.50	72.05	327368.922	6262615.342	TERRA FIRMA GRP	В
02	JUNCTION PIT INLET	1200	900	1550	600	600	70.50	72.05	327369.986	6262614.284	TERRA FIRMA GRP	В
03	JUNCTION PIT OUTLET	1200	900	1870	600	450	70.24	72.11	327284.867	6262530.824	TERRA FIRMA GRP	В
04	JUNCTION PIT OUTLET	1200	900	1870	600	450	70.24	72.11	327285.930	6262529.766	TERRA FIRMA GRP	В
05	GRATED INLET PIT	600	600	550		225	71.50	72.02	327342.643	6262643.257	FLAT GRATE HEEL SAFE	С
06	GRATED INLET PIT	600	600	670	225	225	71.40	72.02	327328.544	6262629.072	FLAT GRATE HEEL SAFE	С
07	GRATED INLET PIT	600	600	770	225	225	71.30	72.02	327314.444	6262614.888	FLAT GRATE HEEL SAFE	С
08	GRATED INLET PIT	600	600	870	225	300	71.20	72.02	327297.219	6262601.811	FLAT GRATE HEEL SAFE	С
09	GRATED INLET PIT	600	600	740	300	300	71.11	71.85	327284.382	6262588.408	FLAT GRATE HEEL SAFE	С
10	GRATED INLET PIT	600	600	880	300	300	71.01	71.85	327272.921	6262572.833	FLAT GRATE HEEL SAFE	С
11	GRATED INLET PIT	900	900	2750	300	375	69.14	71.85	327259.060	6262558.837	FLAT GRATE HEEL SAFE	С
12	BIO-BASIN OUTLET	900	900	1100	150	450	69.34	70.49	327299.213	6262512.845	SURCHARGE GRATE	В
13	JUNCTION PIT	1200	900	2930	450	450	69.16	72.11	327287.413	6262528.156	TERRA FIRMA GRP	В

Notes: Install uPVC drain at 1:200 gradient from Pit 05 to Pit 11.

Refer drawing 012 for installation details of pits 01 & 02

Refer drawing 013 for installation details of pits 03 and 04

Pit 011 to be fitted with step irons

Pit heights to match revised path & grated drain design design. Levels may alter slightly on-site to suit

TurfOne
A BildGroup Company



CONSTRUCTION ISSUE

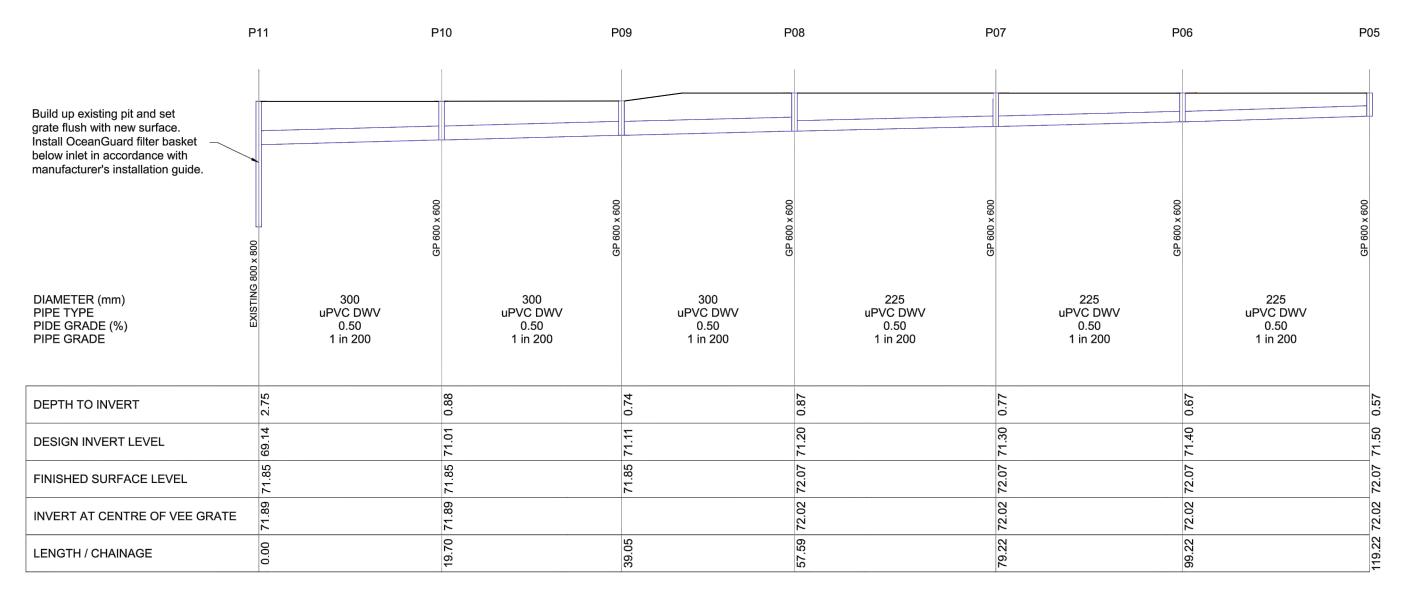
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KU-RING-GAI COUNCIL
PROJECT:
PROPOSED STORMWATER MITIGATION AND
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS
OVAL DESIGN AND CONSTRUCT

DRAWING TITLE:
STORMWATER LONG SECTIONS & PIT
SCHEDULE SHEET 1

JOB NO: TO-003 SHEET: 009 REV: A7



NOTE: ALL PITS TO BE FITTED WITH OCEANGUARD FILTER BASKETS BELOW INLET IN ACCORDANCE WITH MANUFACTURER'S INSTALLATION GUIDE NOTE: PIT HEIGHTS TO MATCH REVISED PATH & GRATED DRAIN DESIGN. DESIGN LEVELS MAY ALTER SLIGHTLY ON-SITE TO SUIT

Confirmation on Oceanguard pit install required. Requirements in REF to be met.







CONSTRUCTION ISSUE	
23	

REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
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PROJECT:	SHEET 2
PROPOSED STORMWATER MITIGATION AND	
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS	

OVAL DESIGN AND CONSTRUCT

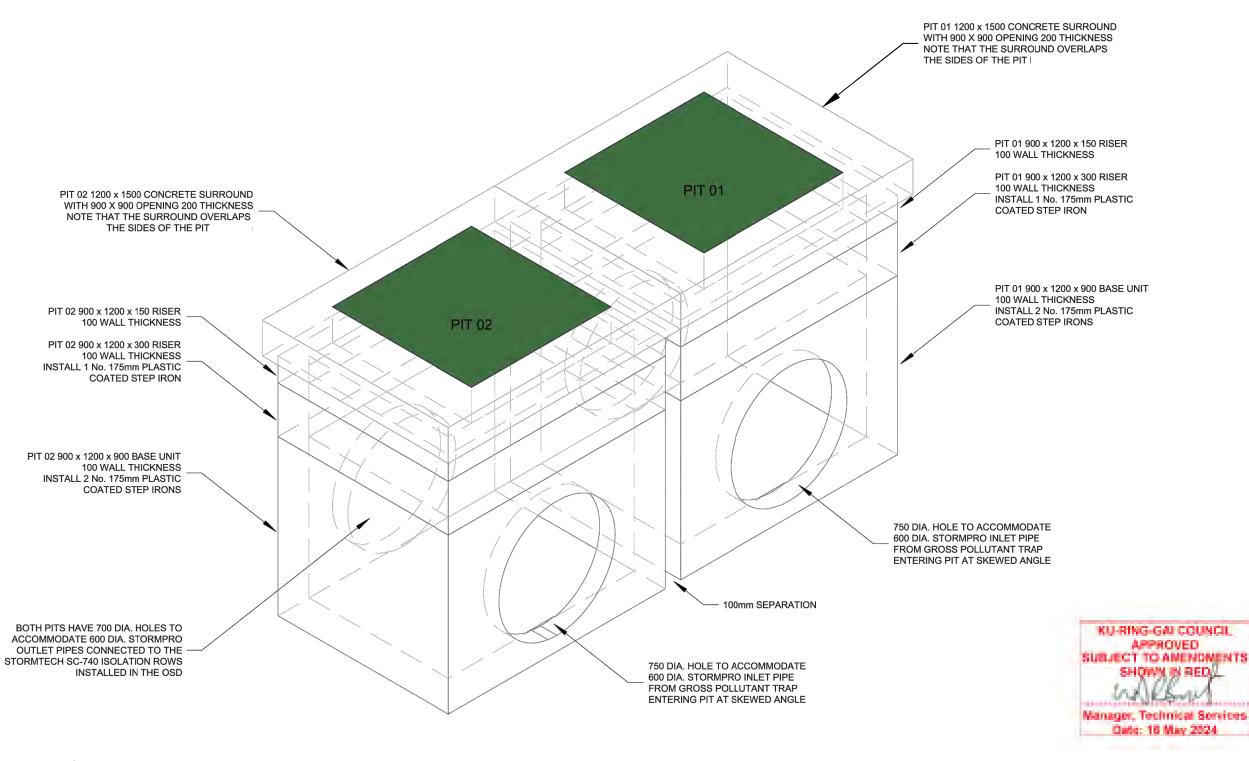
STORMWATER LONG SECTIONS
SHEET 2

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JOB NO: TO-003

SHEET: 010

REV: A7



ISOMETRIC VIEW

NOT TO SCALE

VIEWED FROM INLET SIDE (NOTIONALLY THE EASTERN SIDE)

NOTES: THESE PITS ARE NOT SYMETRICAL. INLET HOLES ARE 750 DIA., OUTLET HOLES ARE 700 DIA. PIT COVERS ARE TO BE TERRA FIRMA B80 1055 x 1055 jct GREEN FRP CLASS B TO SUIT 900 x 900 CLEAR OPENING





CONCERNICENCY
CONSTRUCTION ISSUE

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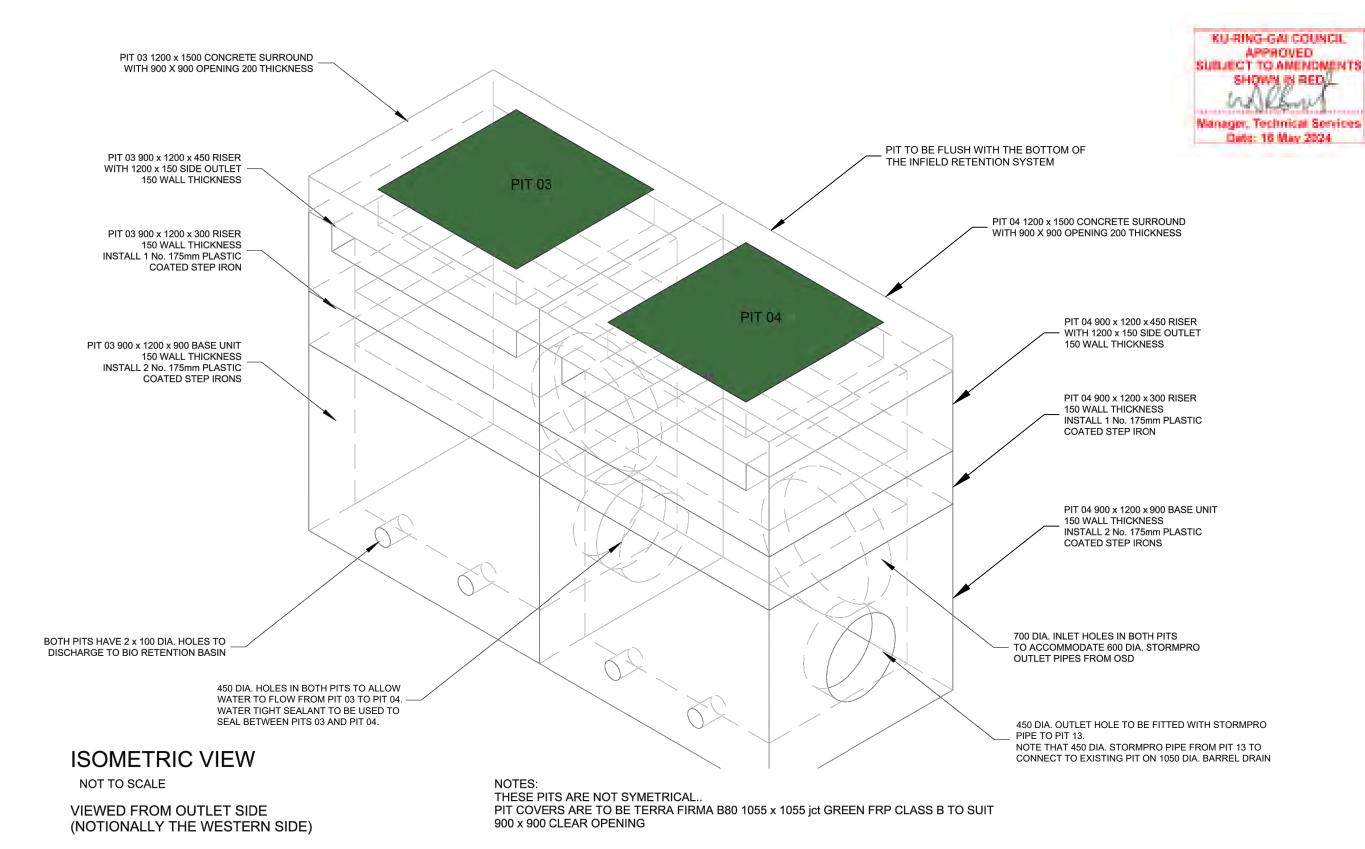
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PROPOSED STORMWATER MITIGATION AND SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS OVAL DESIGN AND CONSTRUCT

SPORTS FIELD INLET PITS DETAILS SHEET 1

JOB NO: TO-003

SHEET: 011







CONSTRUCTION ISSUE

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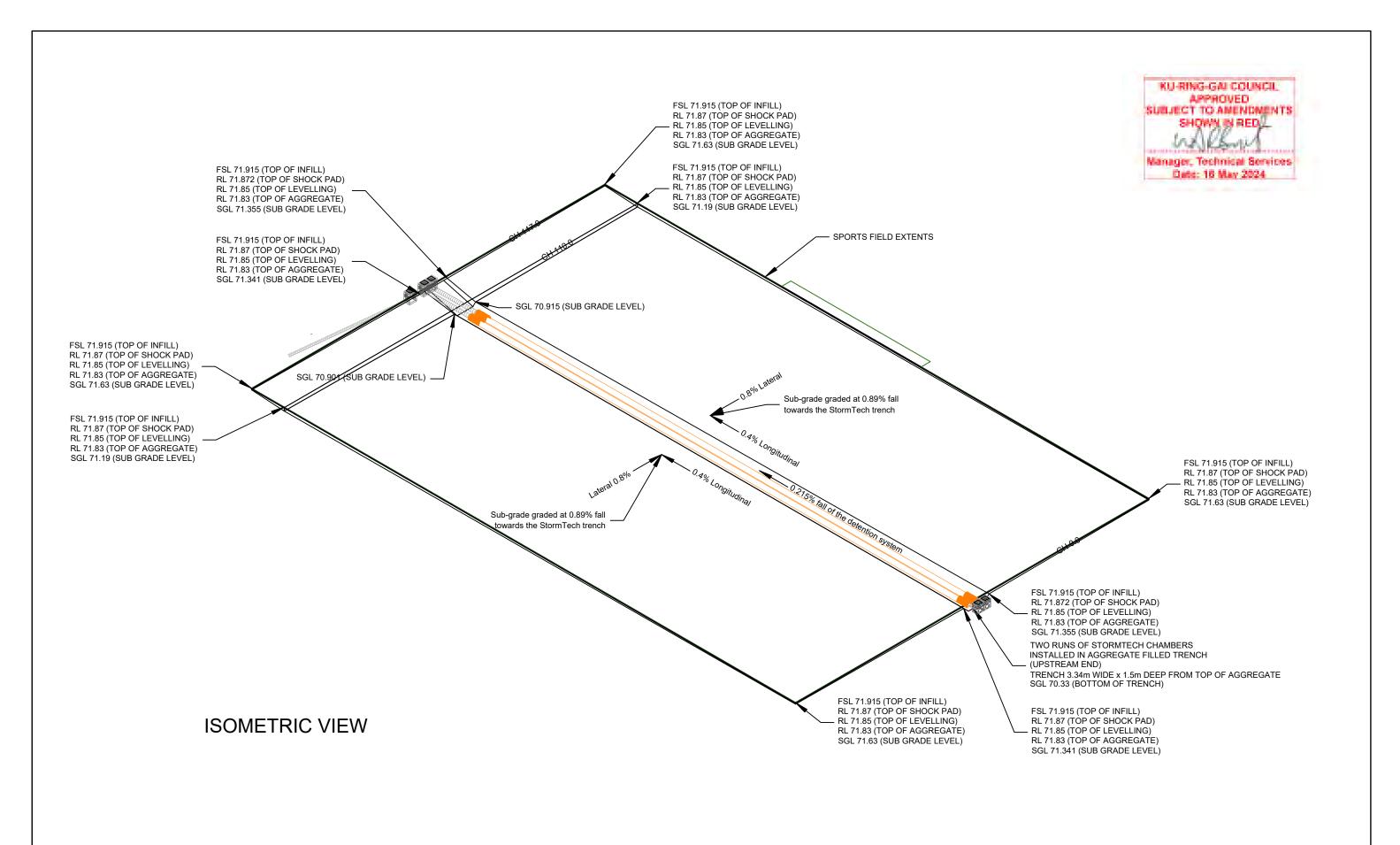
KU-RING-GAI COUNCIL

PROJECT:
PROPOSED STORMWATER MITIGATION AND
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS
OVAL DESIGN AND CONSTRUCT

JOB NO:

DRAWING TITLE:
SPORTS FIELD INLET PITS DETAILS SHEET 2

JOB NO: TO-003 SHEET: 012







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DRAWING TITLE:

ON-SITE DETENTION ISOMETRIC LAYOUT

PROPOSED STORMWATER MITIGATION AND
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS
OVAL DESIGN AND CONSTRUCT

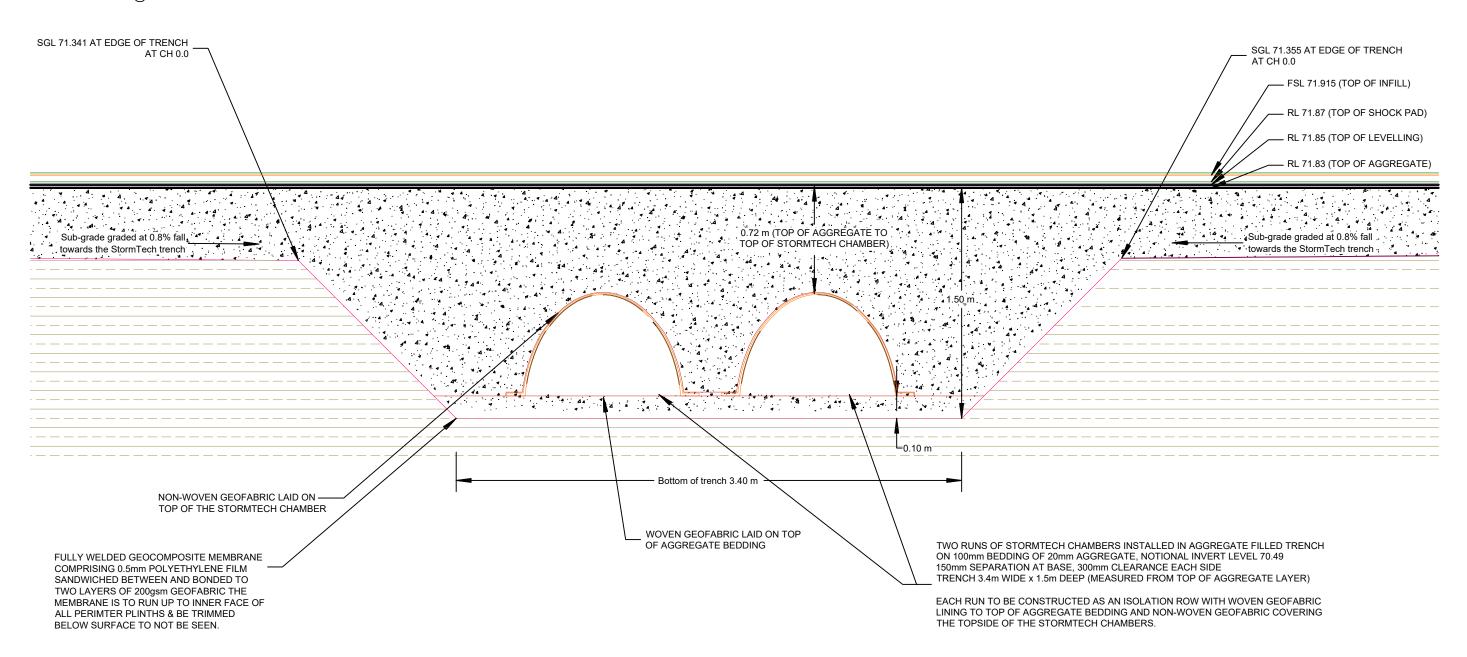
JOB NO: TO-003 SHEET: 013

KU-RING-GAI COUNCIL APPROVED: SUBJECT TO AMENDMENTS SHOWN IN RED. Date: 16 May 2024

Query still unanswered on the 100mm beneath the chambers - to confirm prior to install

SECTIONAL VIEW OF STORMTECH TRENCH AT CH 1.0

SCALE 1:25 @ A3







CONSTRUCTION ISSUE

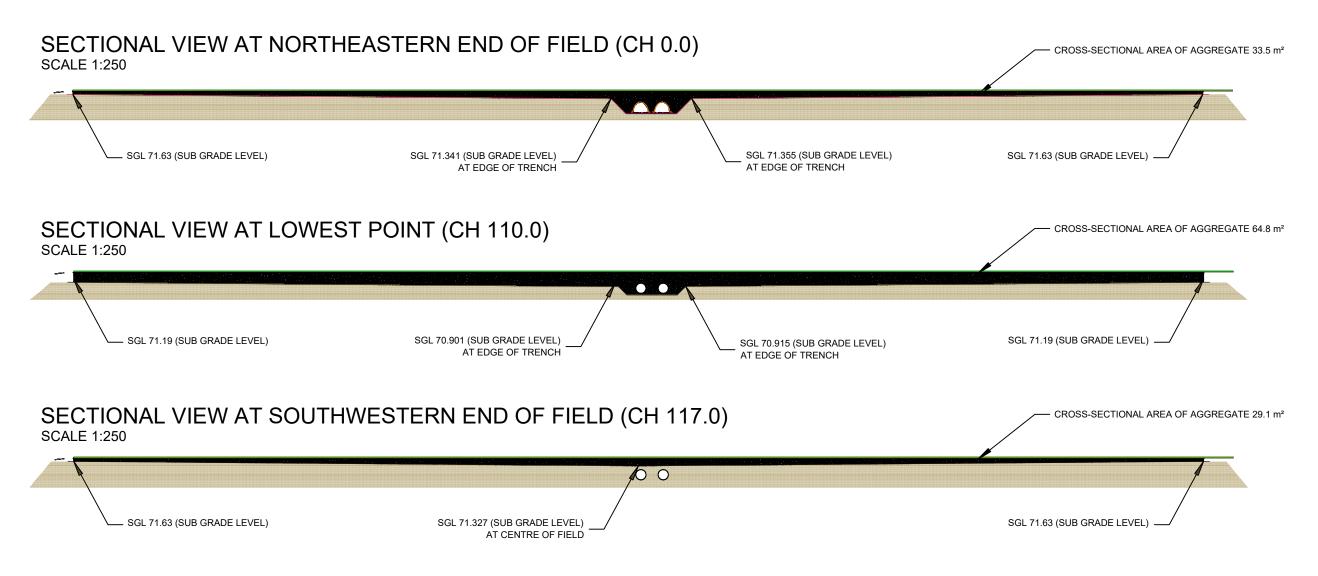
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DJECT:	

ING-GAI COUNCIL	ON-SITE DETENTION PROFILE SECTION
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PROPOSED STORMWATER MITIGATION AND
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS
OVAL DESIGN AND CONSTRUCT

DRAWING TITLE:



VOLUMETRIC CALCULATION FOR ON-SITE DETENTION

Cross-sectional area of aggregate:

CH 0.0 33.5 m² CH 110.0 64.8 m² CH 117.0 29.1 m²

Volume of aggregate CH 0.0 to CH 110 = $110 \times (33.5 + 64.8) / 2 = 5,406 \text{ m}^3$ Volume of aggregate CH 110.0 to CH 117.0 = $7 \times (64.8 + 29.1) / 2 = 328 \text{ m}^3$

Therefore total volume of aggregate = 5,734 m³

Void space in aggregate layer = 0.4 x 5,734 = 2,293 m³

Void space in StormTech chambers = $110 \times 1.30 = 143 \text{ m}^3$

Void space in 600 dia. StormPro pipes = 12.0m x 0.28 = 3.36 m³

Therefore total void space measured to underside of blinding layer = 2,439.36 m³

Capacity of on-site detention = 2.44 megalitres







CONSTRUCTION ISSUE	

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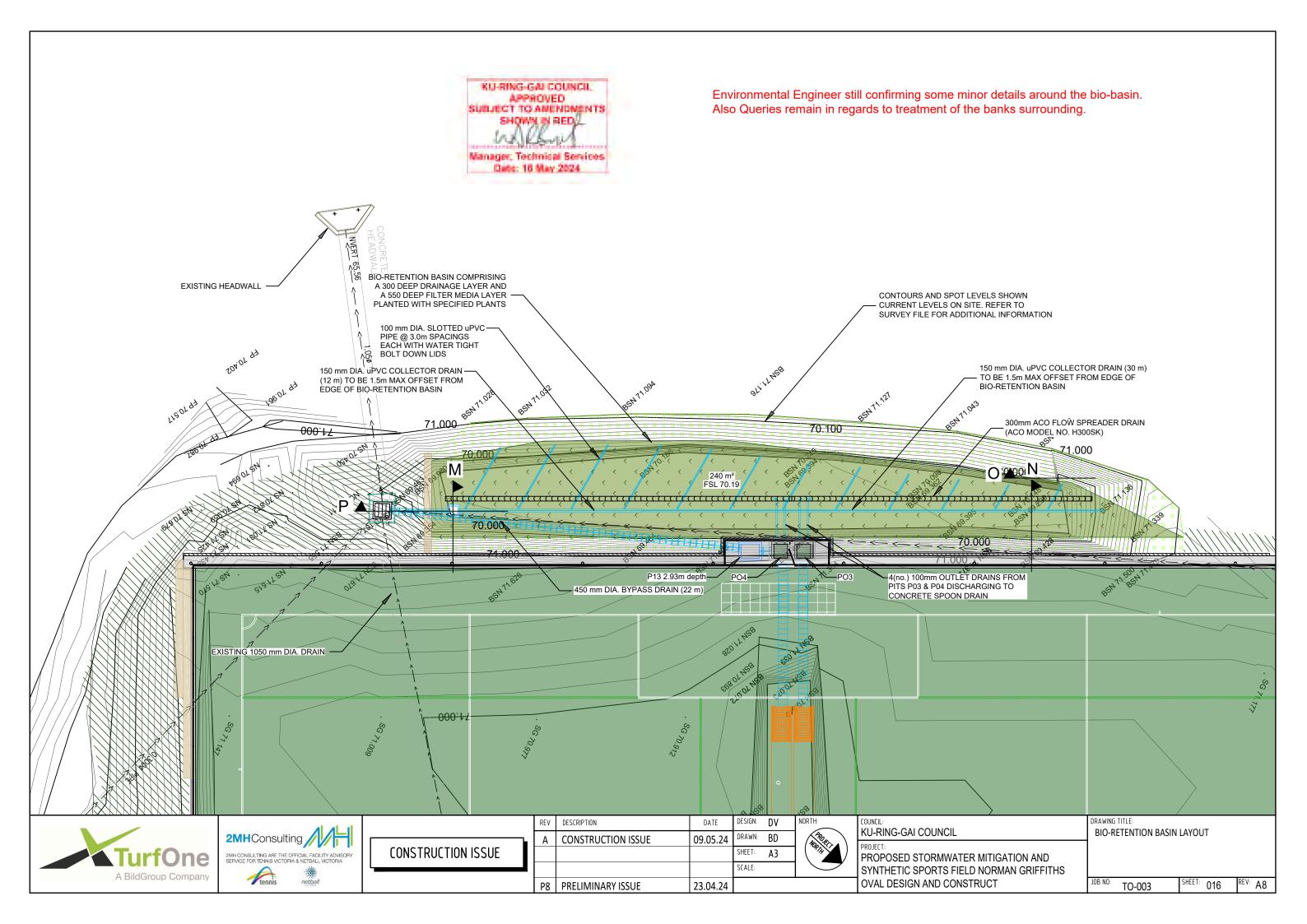
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KU-RING-GAI COUNCIL

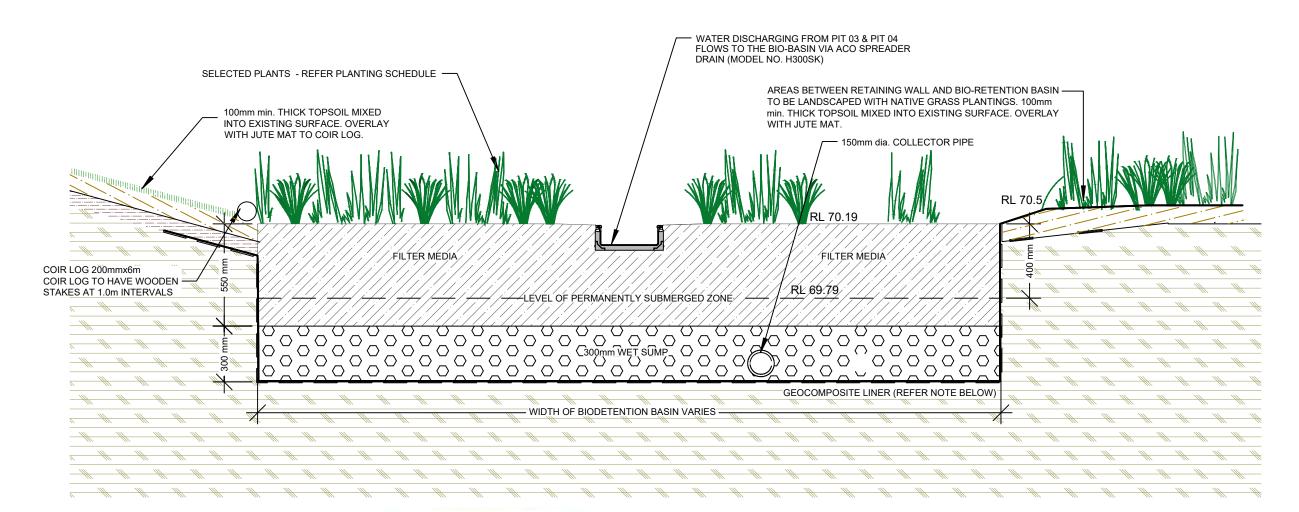
PROJECT:

PROPOSED STORMWATER MITIGATION AND SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS OVAL DESIGN AND CONSTRUCT

DRAWING TITLE:
ON-SITE DETENTION CALCULATIONS &
SECTIONAL VIEWS

JOB NO: TO-003 SHEET: 015 REV: A7





SCHEMATIC SECTION

SCALE 1:20 @ A3

KU-RING-GAI COUNCIL
APPROVED
SUBJECT TO AMENDMENTS
SHOWN IN RED

Manager, Technical Services
Date: 16 May 2024

Final sing-off required by Environmental Engineer

II TER MEDIA

Filter media is to be a low nutrient freely draining sandy loam. Media infiltration rate: 300mm/hr hydraulic conductivity (saturated).

WET SUMP

Drainage layer is to be 5-7mm clean drainage gravel (not recycled)

GEOCOMPOSITE LINER

Fully welded impermeable geocomposite liner comprising 500 micron polyethylene film sandwiched between and bonded to two layers of non-woven 200 gsm geofabric. Note that this material is the same as the liner to be installed under the OSD. Liner fabric to be pinned to existing ground with 100mm pins. Where required heavy duty geofabric (Bidum A64 or approved similar) to be placed under liner to protect form sharp edges/rocks.

PLANTING SCHEDULE				
BIORETENTION FILTER SURFACE (240 m²)	PLANT SPECIES	SIZE	NUMBER	
	Ficina nodulosa	Tube	380	
	Carex appressa	Tube	380	
	Dianella revoluta	Tube	310	
Density: 8 plants/sq.m	Juncus usitatus	Tube	380	
	Centella asiatica	Tube	190	
	Crinum penduculatum	Tube	190	
	Pratia purpurascens	Tube	90	
		Total	1,920	





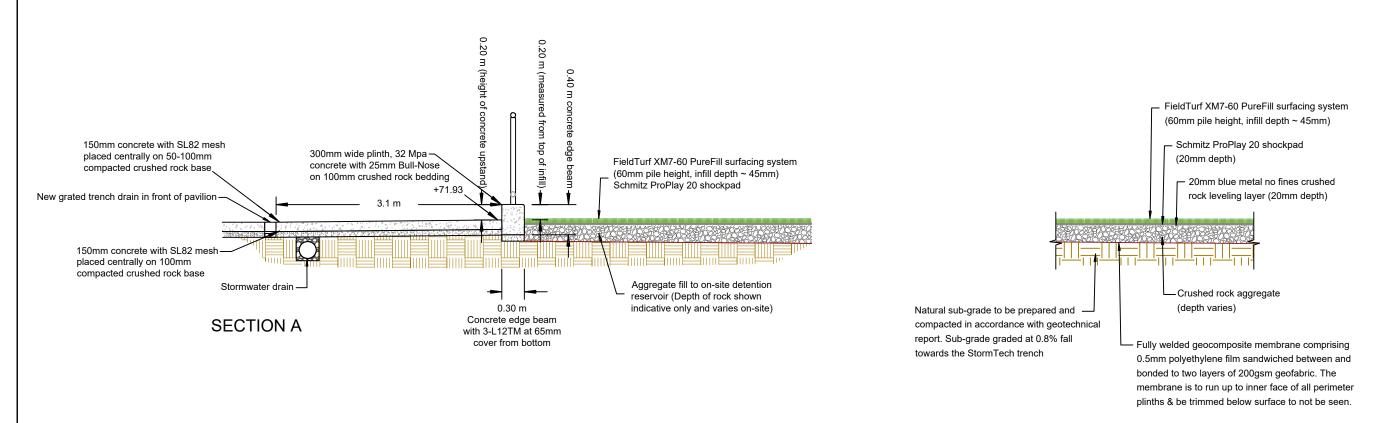
CONSTRUCTION ISSUE

	REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
L	Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
				SHEET:	A3	
				SCALE:		

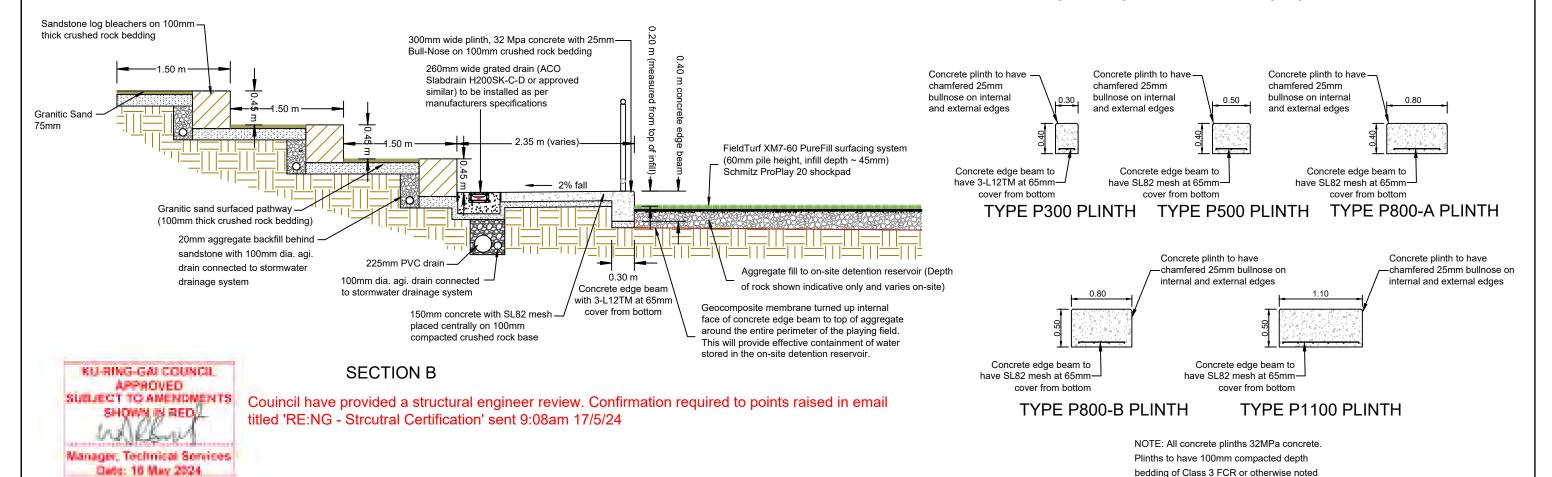
COUNCIL: KU-RING-GAI COUNCIL
PROJECT: PROPOSED STORMWATER MITIGATION AND
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS
OVAL DESIGN AND CONSTRUCT

DRAWING TITLE:
BIO-RETENTION SECTION DETAIL & PLANTING
SCHEDULE

HS JOB NO: TO-003 SHEET: 017 REV: A7



TYPICAL PITCH PAVEMENT SECTION







CONSTRUCTION ISSUE

REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
			SHEET:	A3	
			SCALE:		

COUNCIL:

KU-RING-GAI COUNCIL

PROJECT:

PROJECT:

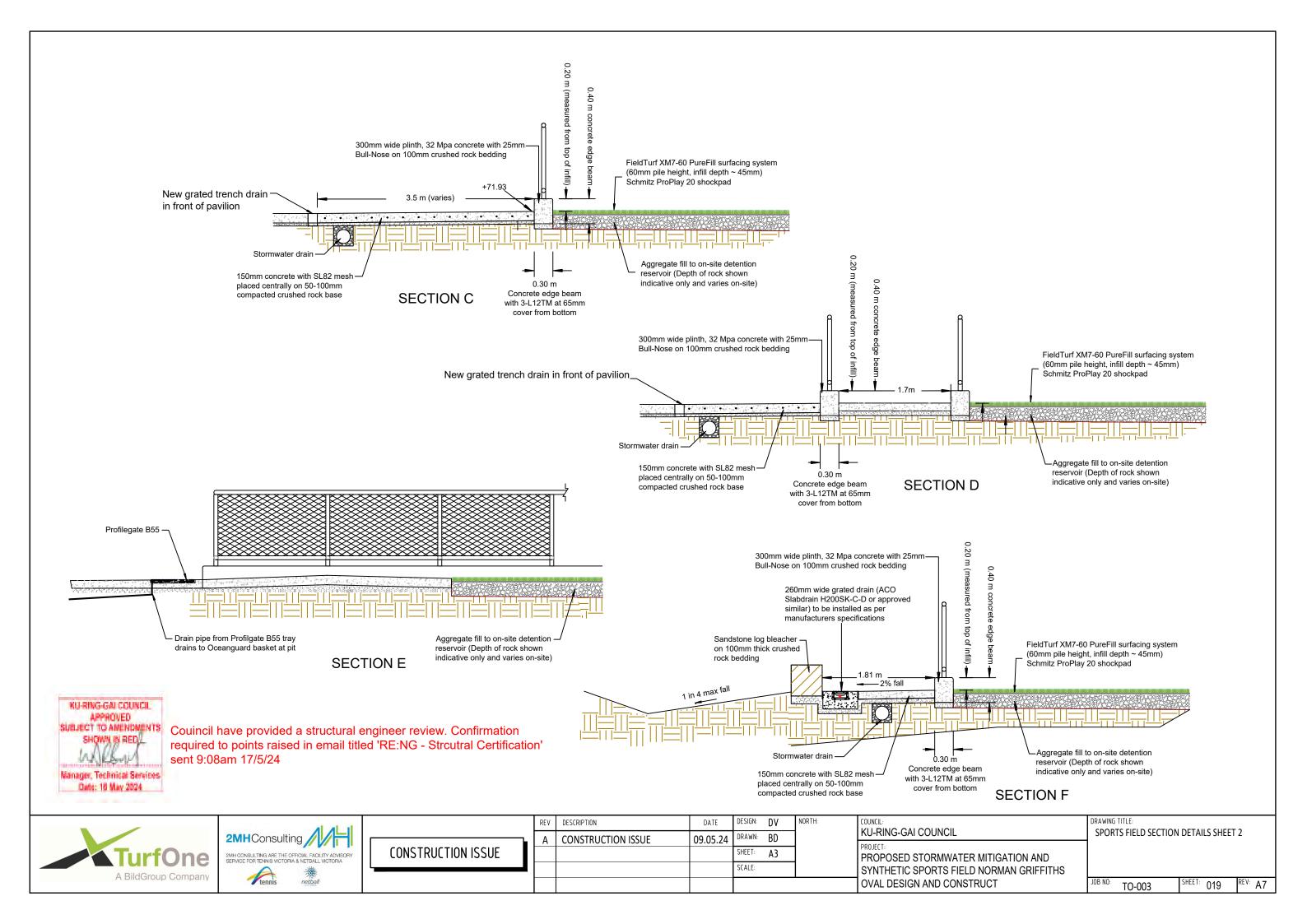
PROJECT:

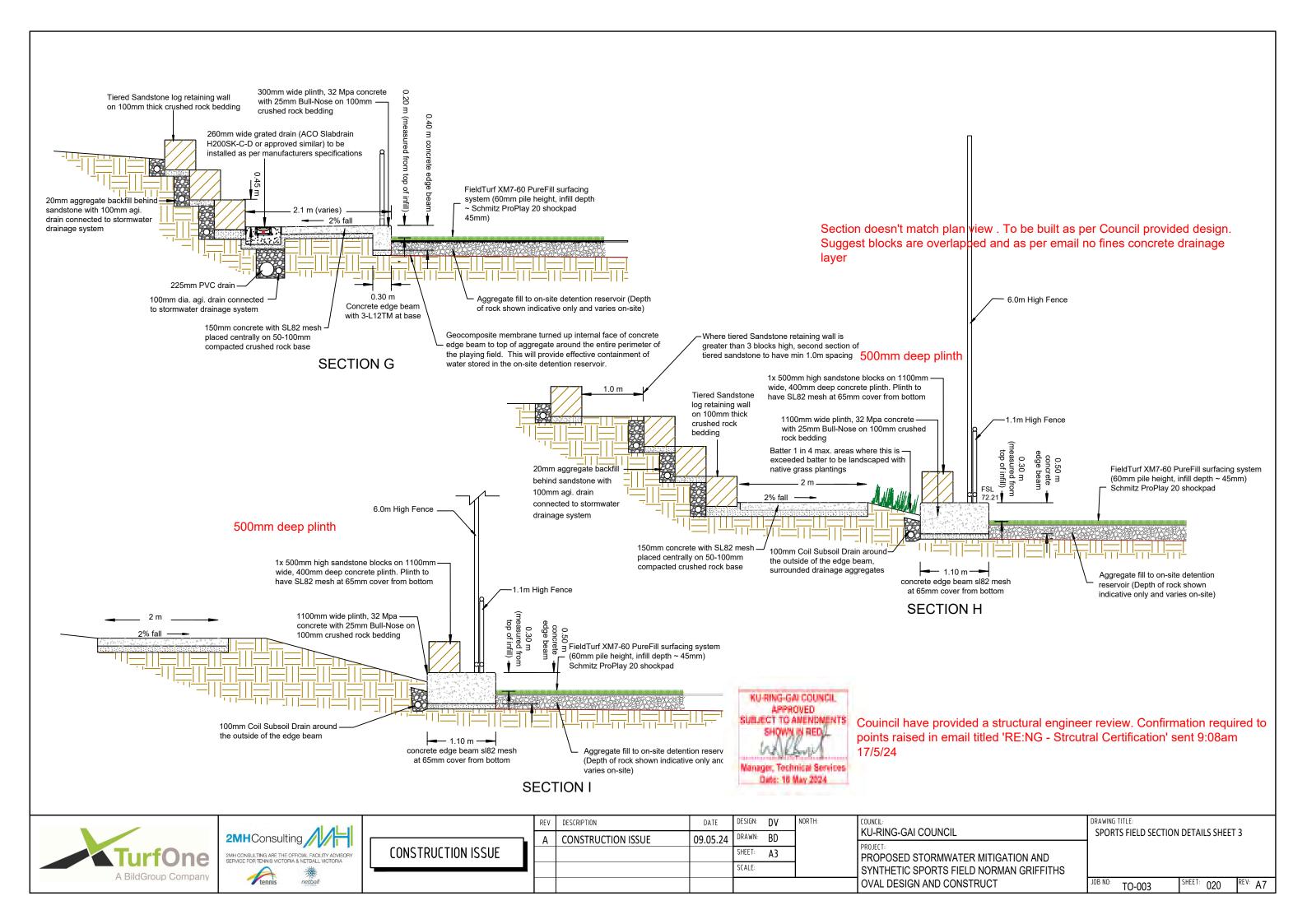
PROPOSED STORMWATER MITIGATION AND

PROJECT:
PROPOSED STORMWATER MITIGATION AND
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS
OVAL DESIGN AND CONSTRUCT

SPORTS FIELD SECTION DETAILS SHEET 1

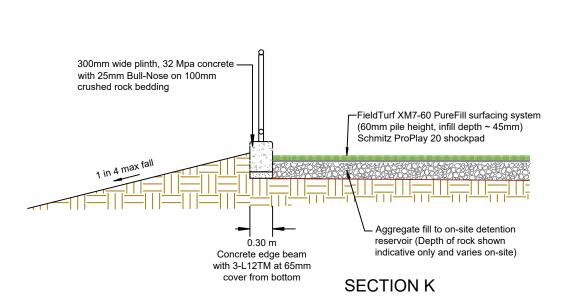
JOB NO: TO-003 SHEET: 018

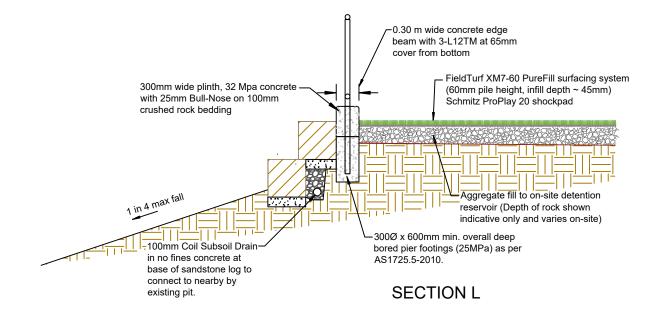




Will be unable to be built as shown below - levels/requirments of overland flow path to be met 6.0m High Soft Mesh Netting 1x 500mm high sandstone blocks on 800mm wide, 400mm deep concrete plinth on 100mm crushed rock bedding. Plinth to have sl82 mesh at 65mm cover from -1.1m High Fence FieldTurf XM7-60 PureFill surfacing system FSL 72.5 top plinth 2.8m approx width to invert (60mm pile height, infill depth ~ 45mm) FSL 72.21 Schmitz ProPlay 20 shockpad (width varies) Aggregate fill to on-site detention reservoir (Depth of rock shown indicative only and Blocks to be binded to plinth -0.80 m with mortar or suitable product varies on-site) Concrete edge beam to reduce water ingress. with sl82 mesh at 65mm cover from bottom

SECTION J







SUBJECT TO AMENDMENTS Couincil have provided a structural engineer review. Confirmation required to points raised in email titled 'RE:NG - Strcutral Certification' sent 9:08am 17/5/24

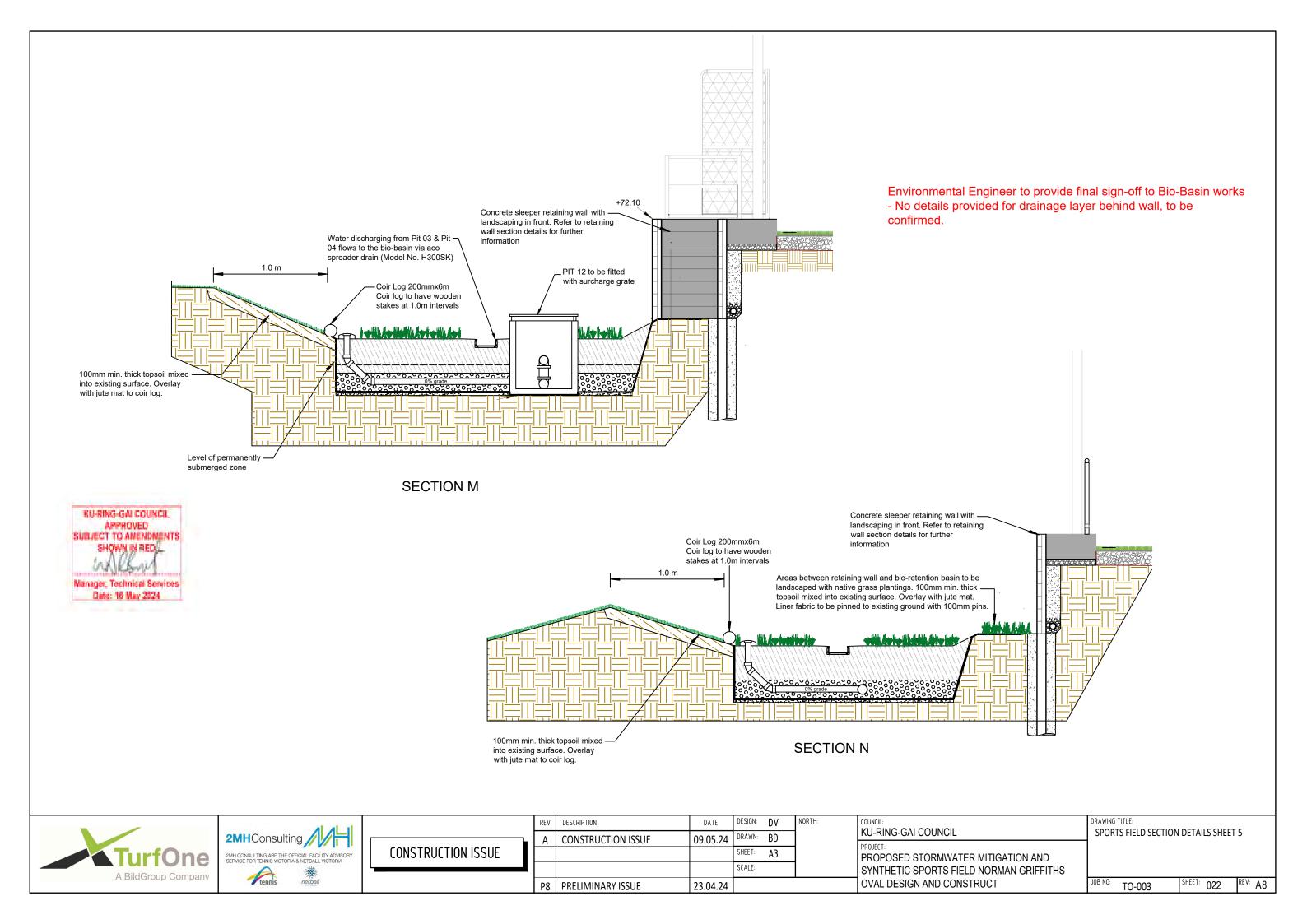


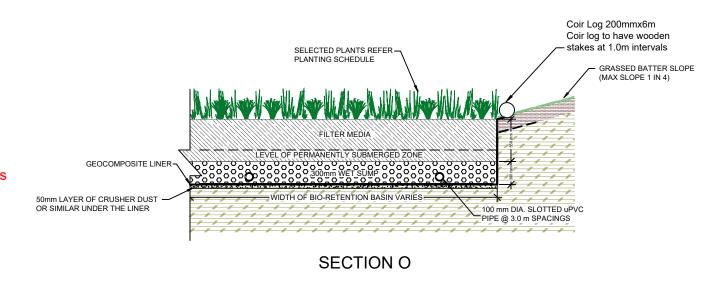


CONSTRUCTION ISSUE	
CONSTRUCTION ISSUE	

	REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
	Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
				SHEET:	A3	
l				SCALE:		
	P8	PRELIMINARY ISSUE	23.04.24			

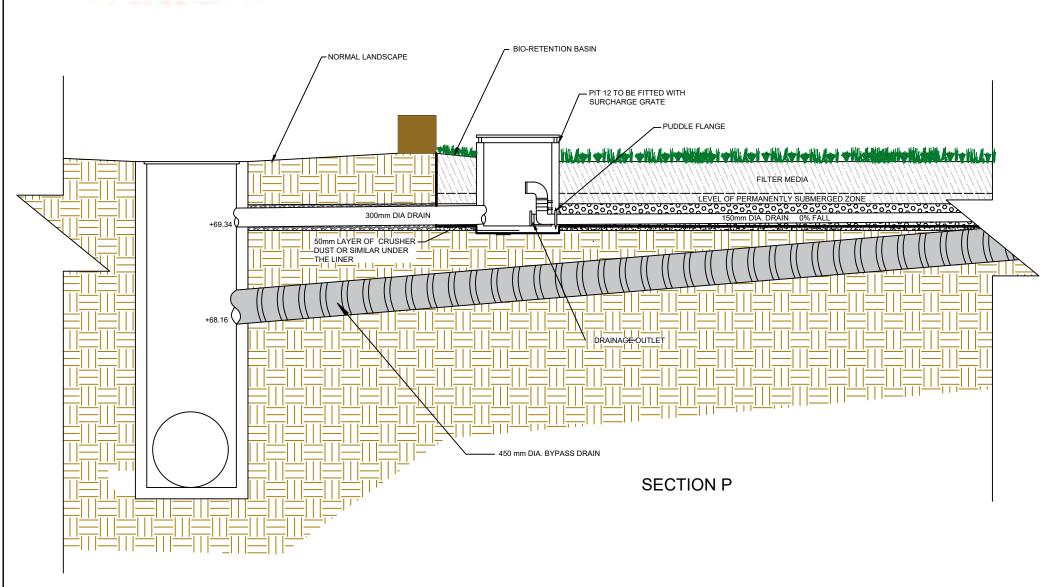
COUNCIL: KU-RING-GAI COUNCIL	DRAWING TITLE: SPORTS FIELD SECTION DETAILS SHEET 4	
PROJECT: PROPOSED STORMWATER MITIGATION AND SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS		
OVAL DESIGN AND CONSTRUCT	JOB NO: TO-003 SHEET: 021 RE	ĒV





KU-RING-GALCOUNCIL APPROVED SUBJECT TO AMENDMENTS Manager, Technical Services Date: 16 May 2024

Environmental Engineer to provide final sign-off to Bio-Basin works







C	ONSTRUC	TION ISSUE	

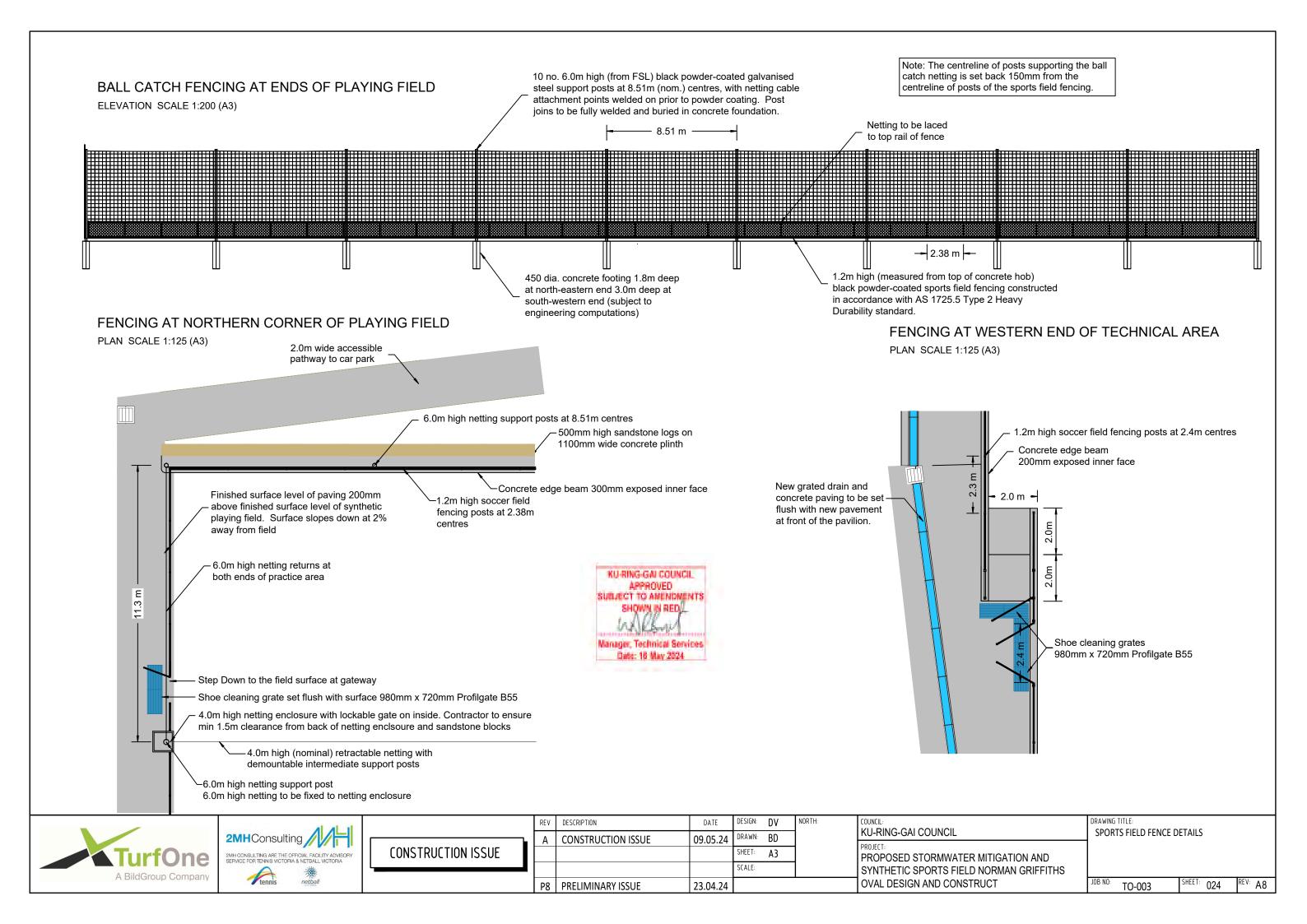
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	Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
				SHEET:	A3	
l				SCALE:		
	P8	PRELIMINARY ISSUE	23.04.24			

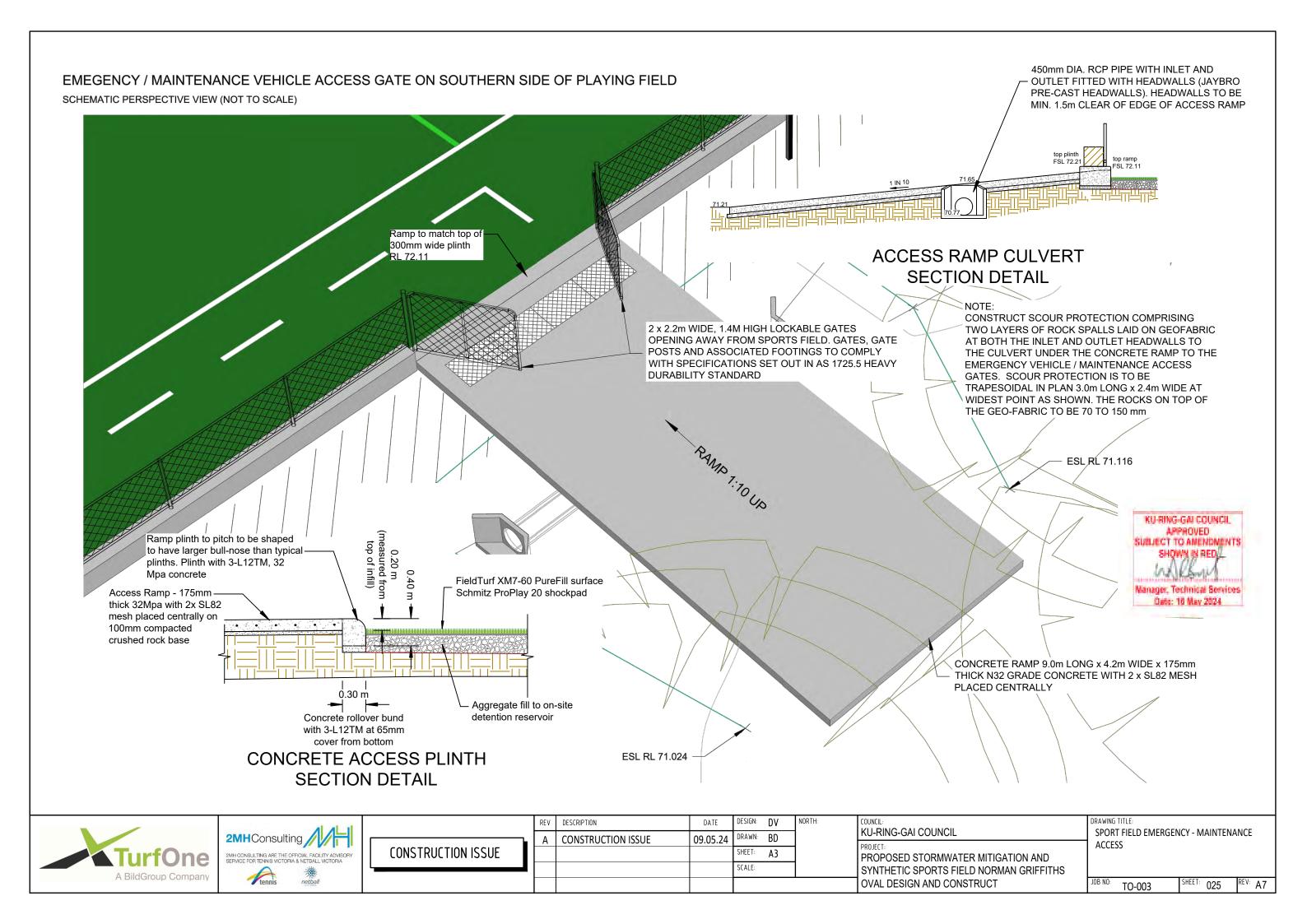
COUNCIL:	DRAWING 7
KU-RING-GAI COUNCIL	SPORT
PROJECT:	
PROPOSED STORMWATER MITIGATION AND	
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS	
OVAL DESIGN AND CONSTRUCT	JOB NO:

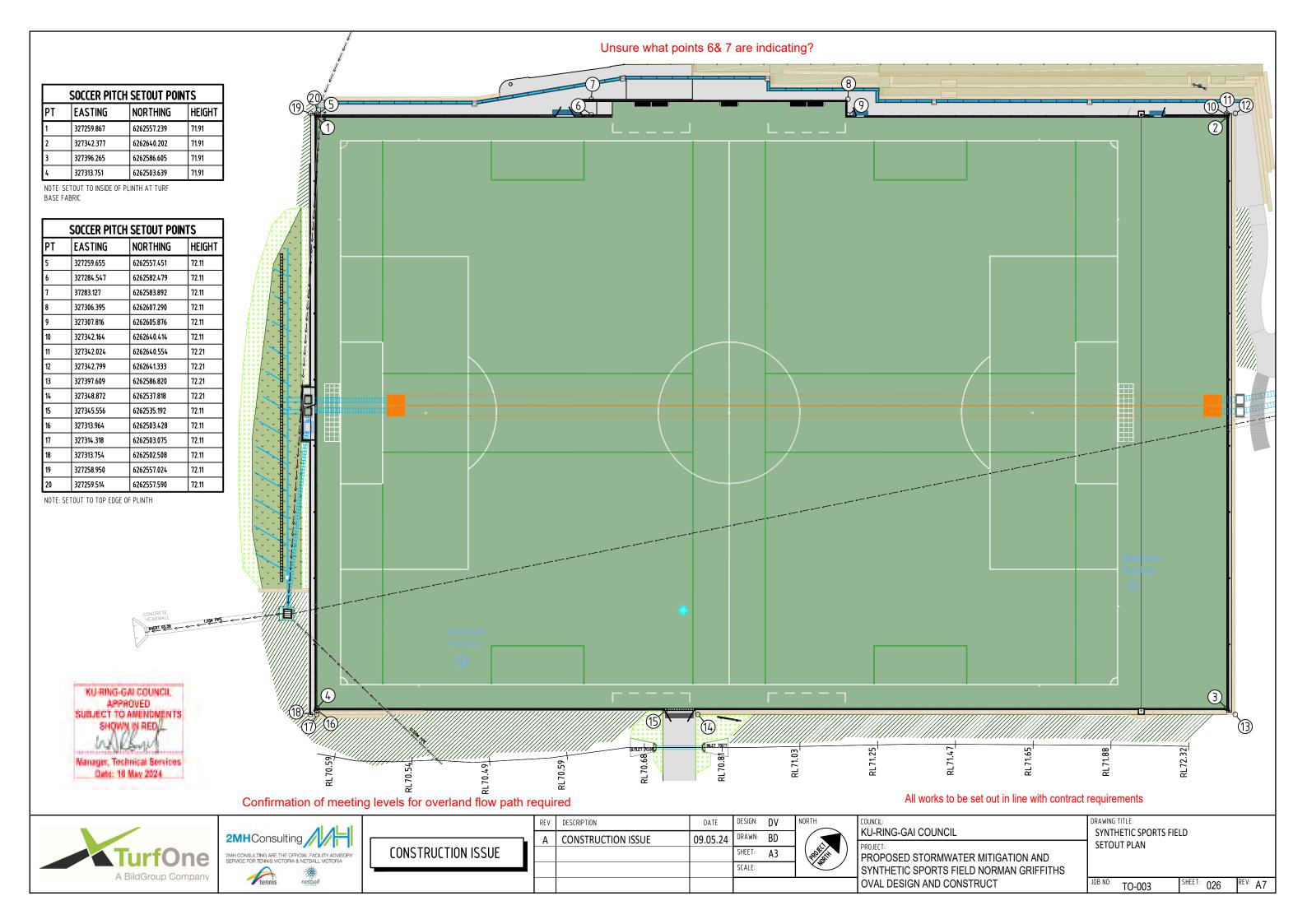
DRAWING TITLE: ORTS FIELD SECTION DETAILS SHEET 6

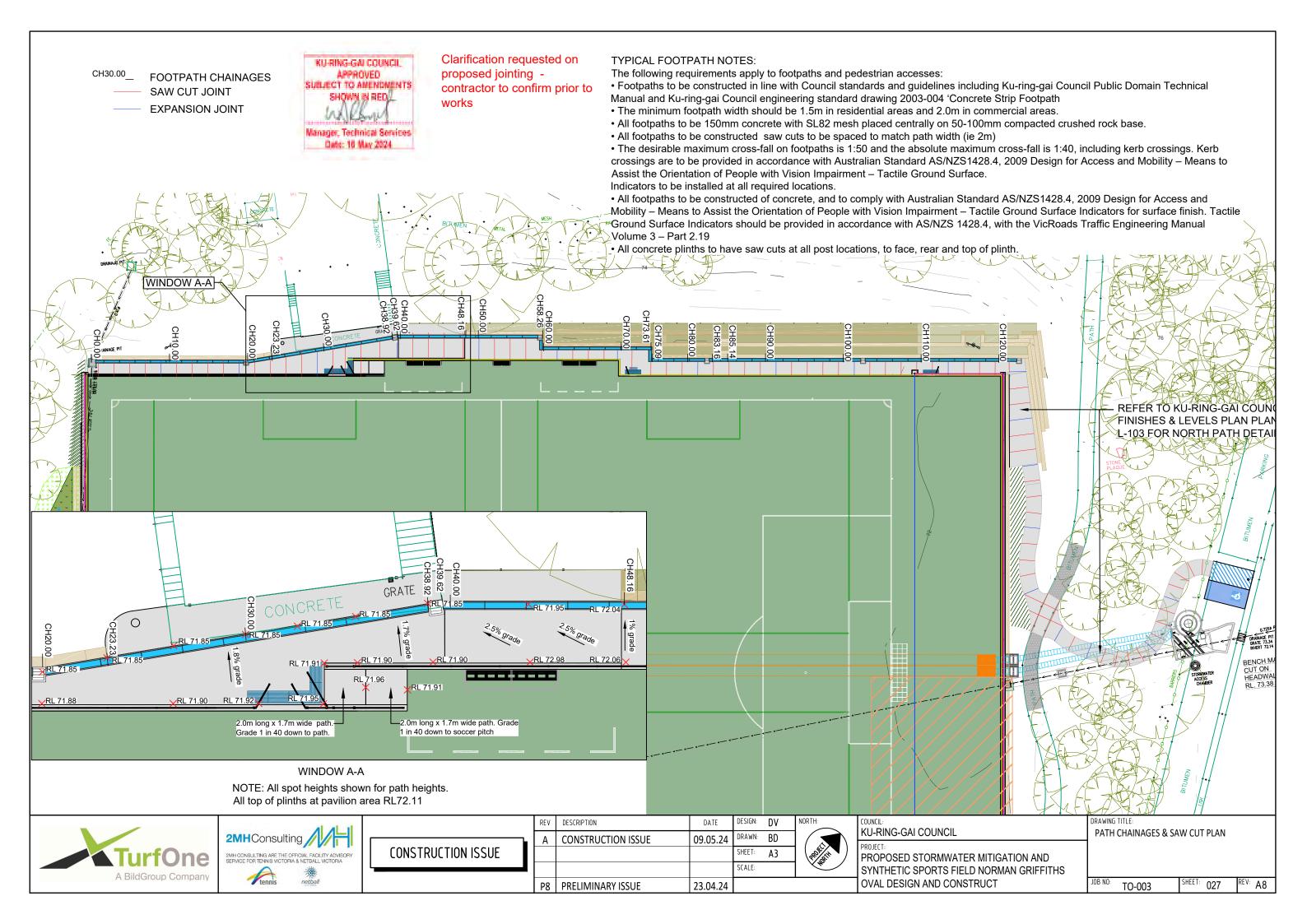
OVAL DESIGN AND CONSTRUCT

SHEET: 023 TO-003 REV: A8











		/	ı					-				1	_				_		<u> </u>				_	
		·				IP /1.85		——————————————————————————————————————			IP /2.04		IP 72.04 IP 72.05				IF /2:05							
Horiz Curve Data Design Cline Grade (%)				0.00	%			2	.23	%_	0	.00 % <u>0</u> .7	1 9	<u>%</u> 0.00	%	1,2	5 %	,			0.0) %		
DATUM R.L.	66	,							_															
Design Levels	71.85	71.85		71.85	71.85	71.85	71.85	71.85	71.86	72.04	72.04	72.04	72.05		72.05	72.05	72.07	72.07	72.07	72.07		10.71	72.07	72.07
Existing Surface	71.80	72.07		71.69	71.63	71.72	T.B.C	T.B.C	T.B.C	T.B.C	T.B.C	71.96	71.99		71.92	71.95	71.94	71.95	72.00	71.92		00.7	72.02	72.03
Northings	6262559.179	6262566.261		6262573.344	6262575.756	6262581.302	6262588.609	6262589.183	6262589.456	6262595.308		6262602.423			6262608.53	6262611.103	6262610.076	6262613.545	6262615.777	6262611.212		01.7.7000000000000000000000000000000000	6262634.784	6262641.853
Eastings	327258.511	327265.571		327272.631	327274.778	327278.661	327283.777	327284.177	327284.441	327290.128	327291.434	327297.297	327298.503		327305.502	327308.029	327309.092	327312.568	327314.804	201.01.01.02	ם, איכדיינ	00.020	327333.753	327340.827
Chainage	0.00	10.00		20.00	23.23	30.00		39.62	40.00	48.16	50.00	58.26	00.09		70.00	73.61	75.09	80.00	83.16		000		110.00	120.00

Scales Hor 1 : 500 (A3 orig) Ver 1 : 100





CONSTRUCTION ISSUE	

REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
			SHEET:	A3	
			SCALE:		

COUNCIL:
KU-RING-GAI COUNCIL
PROJECT:

OVAL DESIGN AND CONSTRUCT

DRAWING TITLE:
PATH LONGITUDINAL SECTION PROPOSED STORMWATER MITIGATION AND SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS

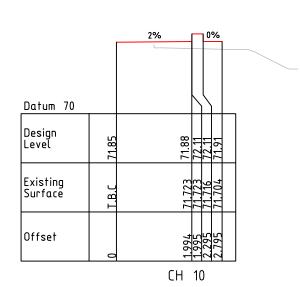
JOB NO: TO-003

REV: A7

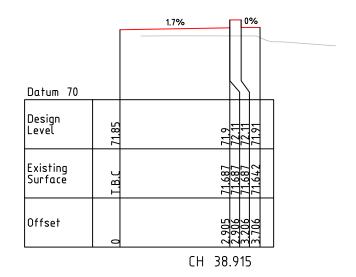
SHEET: 028

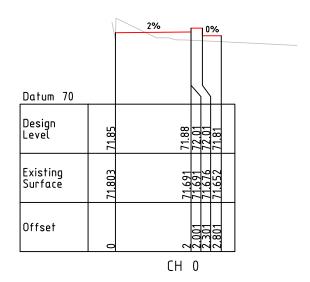


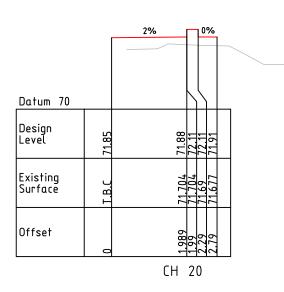
Levels have not been checked to confirm they meet levels provided by Council. Refer to Ku-ring-gai Council Finishes and Levels Plans



Datum 70		2%		0%	
Design Level	71.85	71 88	72.11	71.91	
Existing Surface	T.B.C	£ 77 703	71.703	71.667	
Offset	0	721.	2.175	2.975	
		СН	23.	23	2







	_	1.8%	<u> </u>	%		
Datum 70			/		1	
Design Level	71.85	7191	72.11	71.91		
Existing Surface	T.B.C	71,691	71.691	71.634		
Offset	0	387	3.382 3.682	4.182		
		CH 30			2'	

Scales Hor 1 : 10 (A3 orig) Ver 1 : 10





CONSTRUCTION ISSUE

	REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
	Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
				SHEET:	A3	
l				SCALE:		

COUNCIL:	DRAWING TITLE:
KU-RING-GAI COUNCIL	PATH CROSS
PROJECT:	SHEET 1
PROPOSED STORMWATER MITIGATION AND	
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS	

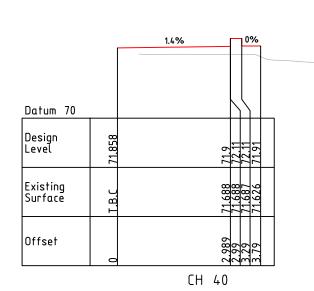
OVAL DESIGN AND CONSTRUCT

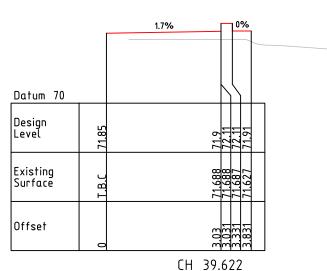
PATH CROSS SECTIONS
SHEET 1

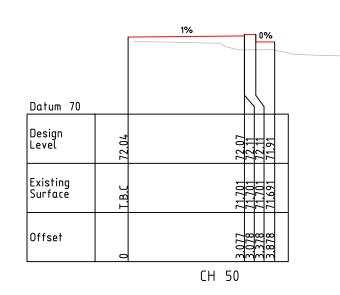
JOB NO: TO-003 SHEET: 029 REV: A7

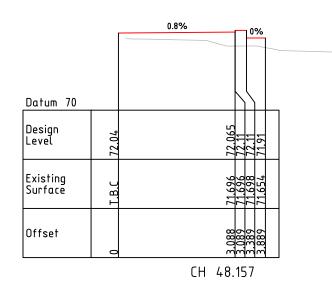


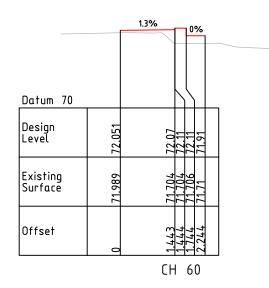
Levels have not been checked to confirm they meet levels provided by Council. Refer to Ku-ring-gai Council Finishes and Levels Plans

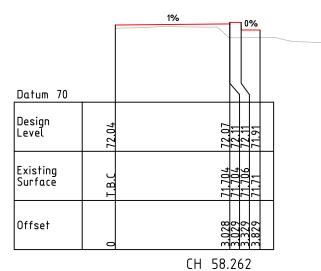












Scales Hor 1 : 10 (A3 orig) Ver 1 : 10





CONSTRUCTION ISSUE

REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
			SHEET:	Α3	
			SCALE:		

COUNCIL:	DRAWING TI
KU-RING-GAI COUNCIL	PATH C
PROJECT:	SHEET 2
PROPOSED STORMWATER MITIGATION AND	
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS	

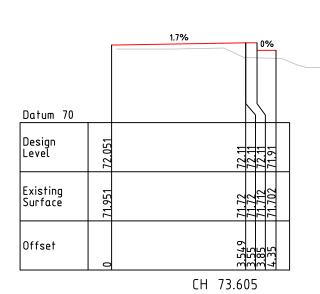
OVAL DESIGN AND CONSTRUCT

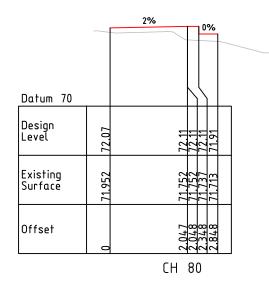
WING TITLE: ITH CROSS SECTIONS IEET 2

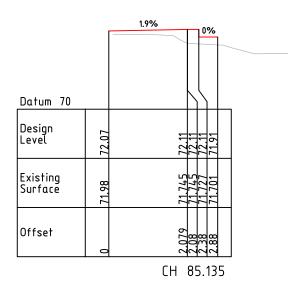
JOB NO: TO-003 SHEET: 030

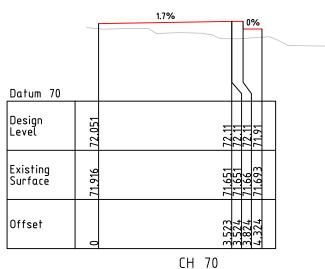


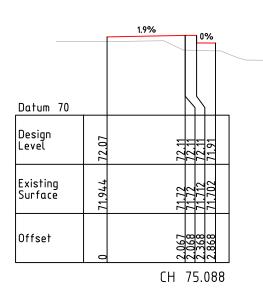
Levels have not been checked to confirm they meet levels provided by Council. Refer to Ku-ring-gai Council Finishes and Levels Plans











Datum 70		2%		09	%			
Design Level	72.07	72 11	72.11	72.11	71.91			
Existing Surface	72.00	8,7,7,	71.748	71.73	71.706			
Offset	0	2 03%	2.035	m	2.835			
		СН	83	3.′	16	-		

Scales (A3 orig) 1 : 100 1 : 100 Hor Ver





CONSTRUCTION ISSUE

REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
			SHEET:	A3	
			SCALE:		

NCIL:	DRAWING TITLE:
J-RING-GAI COUNCIL	PATH CROSS
JECT:	SHEET 3
ROPOSED STORMWATER MITIGATION AND	

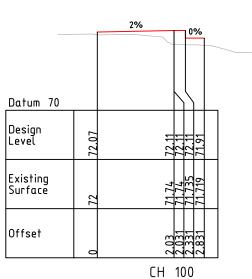
SHEET 3 SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS OVAL DESIGN AND CONSTRUCT

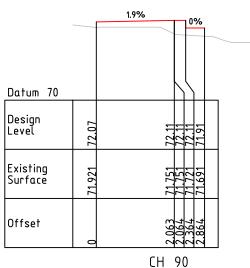
PATH CROSS SECTIONS

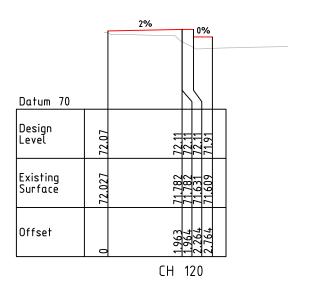
JOB NO: TO-003 SHEET: 031

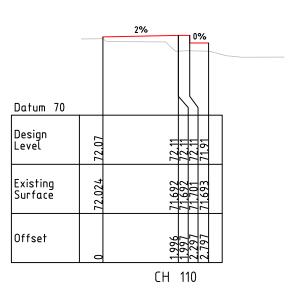












Scales Hor (A3 orig) Ver 1 : 100 1 : 100





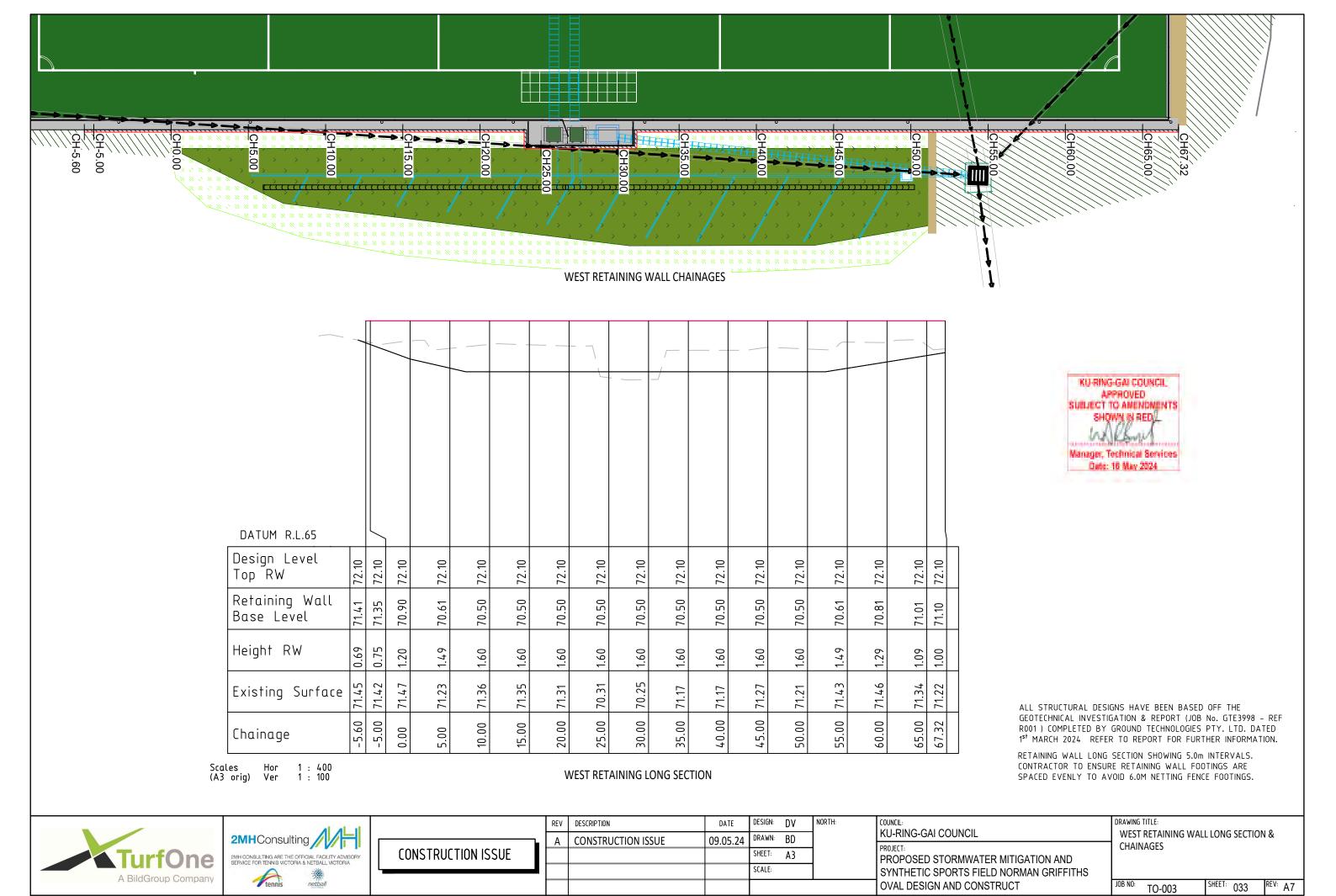
REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
			SHEET:	Α3	
			SCALE:		

COUNCIL:	
KU-RING-GAI COUNCIL	

PROPOSED STORMWATER MITIGATION AND SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS OVAL DESIGN AND CONSTRUCT

DRAWING TITLE: PATH CROSS SECTIONS SHEET 4

JOB NO: <u>TO-003</u> SHEET: 032



SHEET: 033

REV: A7

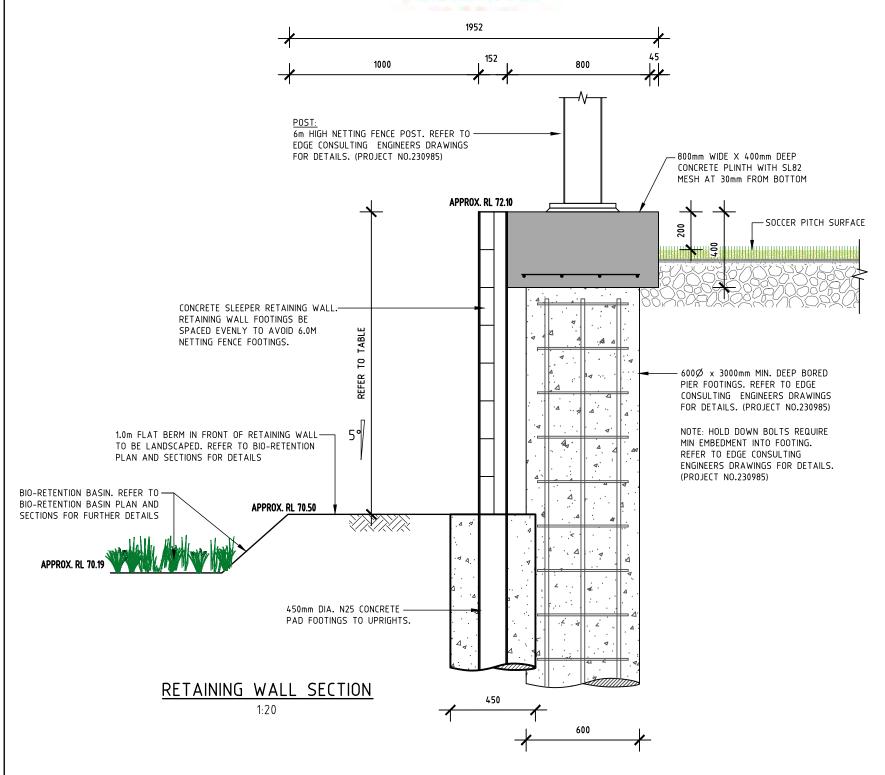
OVAL DESIGN AND CONSTRUCT

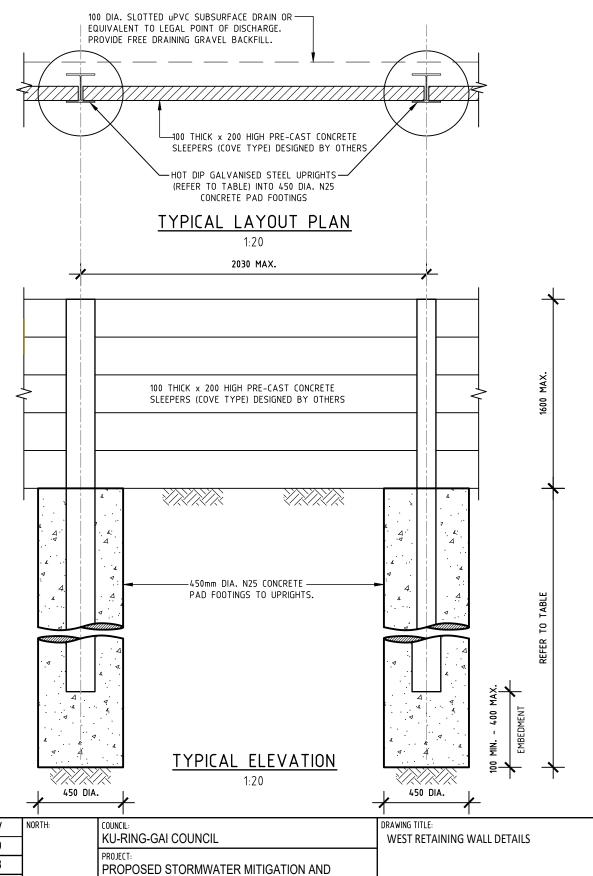
ALL STRUCTURAL DESIGNS HAVE BEEN BASED OFF THE GEOTECHNICAL INVESTIGATION & REPORT (JOB No. GTE3998 - REF R001) COMPLETED BY GROUND TECHNOLOGIES PTY. LTD. DATED 1st MARCH 2024 REFER TO REPORT FOR FURTHER INFORMATION.

KU-RING-GAI COUNCIL
APPROVED
SUBJECT TO AMENDMENTS
SHOWN IN RED
Manager, Technical Services
Date: 18 May 2024

TYPICAL RETAINING WALL DETAILS						
RETAINING HEIGHT	UPRIGHT SIZE	FOOTING DEPTH				
1000mm - 1600mm	150 UC 37 @ 2030mm MAX. CTRS.	450mm DIA. x 2500mm MIN. O/A DEEP, OR FOUNDED 1000mm MIN. INTO SANDSTONE ROCK.				

Still errors on this page as per previous markups





SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS

OVAL DESIGN AND CONSTRUCT

JOB NO:

TO-003

SHEET: 034

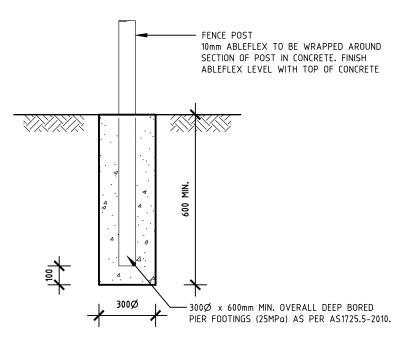
REV: A7





CONSTRUCTION ISSUE

				SCALE:		
1				CCALE		ł
				SHEET:	A3	
	Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
	REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:



TYPICAL 1.2m LOW FENCE INTERMEDIATE POST FOOTING DETAILS 1:20

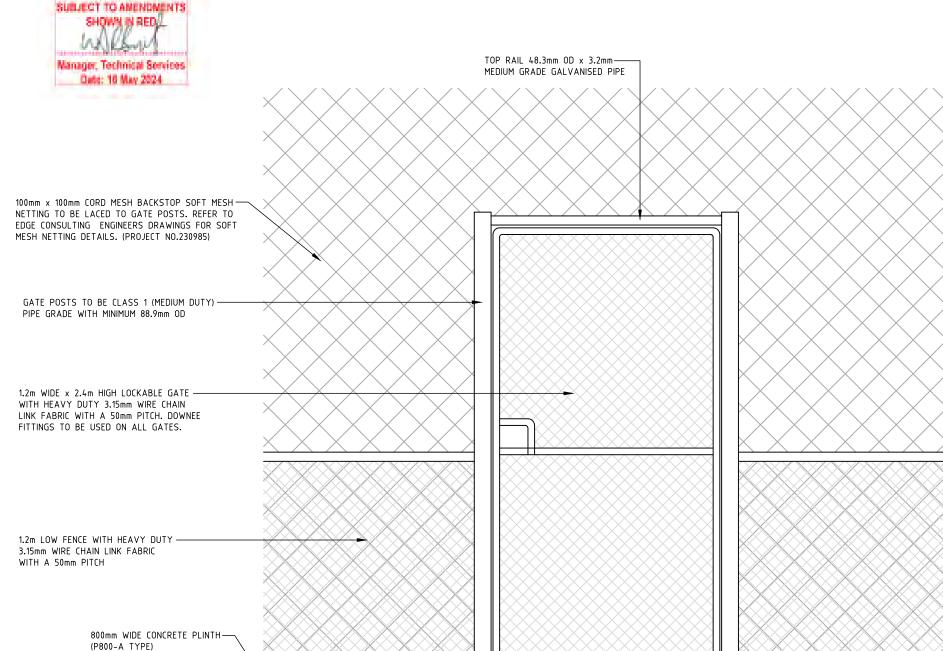
10mm ABLEFLEX TO BE WRAPPED AROUND
SECTION OF POST IN CONCRETE. FINISH
ABLEFLEX LEVEL WITH TOP OF CONCRETE

PROVIDE 1-N16 BAR IN A 'U-SHAPE'
AROUND POST IN BOTH DIRECTIONS
EXTENDING 500mm BACK INTO CONCRETE
PLINTH.

WIDTH VARIES
CONCRETE PLINTH

BORED PIER FOOTING.
REFER TO DETAIL ABOVE FOR FOOTING
DEPTHS

TYPICAL 1.2m LOW FENCE POST FOOTING DETAILS (PLAN VIEW)



1.2m WIDE x 2.4m HIGH ACCESS GATE IN 6.0m SOFT MESH NETTING DETAIL 1:20





CONSTRUCTION ISSUE

KU-RING-GAI COUNCIL APPROVED

	REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
	Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
				SHEET:	Α3	
				SCALE:		
	P8	PRELIMINARY ISSUE	23.04.24			

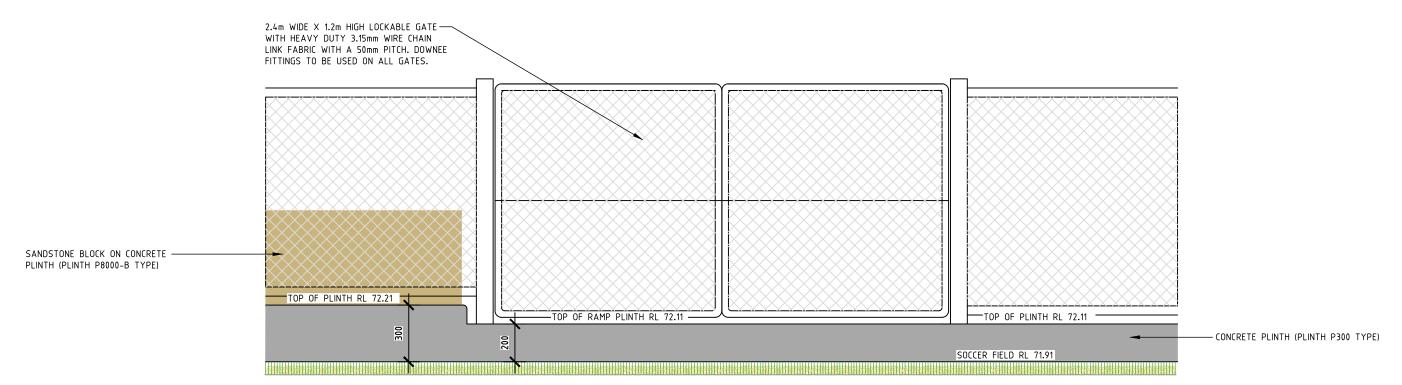
COUNCIL: DRAWING TITLE: WEST GATE

PROJECT:

PROPOSED STORMWATER MITIGATION AND SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS OVAL DESIGN AND CONSTRUCT

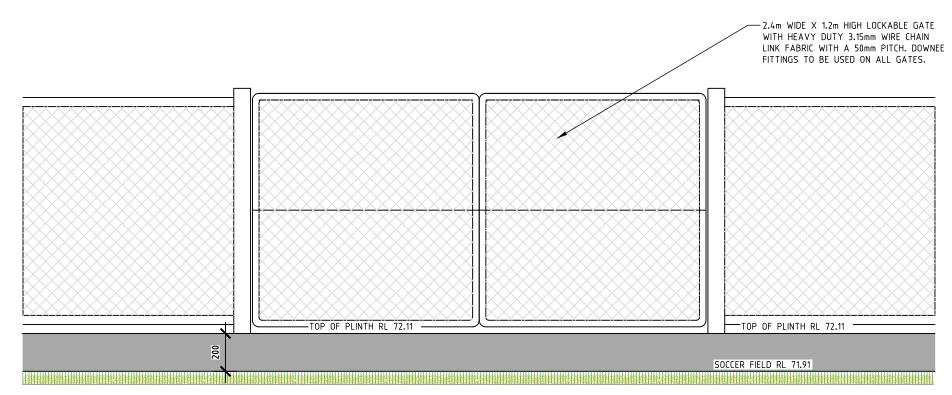
WEST GATE AND LOW FENCE DETAILS

JOB NO: TO-003 SHEET: 035 REV: A8



2.4m WIDE x 1.2m HIGH MAINTENANCE ACCESS GATE DETAIL 1:20

KU-RING-GAI COUNCIL
APPROVED
SUBJECT TO AMENDMENTS
SHOWN IN RED
Manager, Technical Services
Date: 16 May 2024



2.4m WIDE x 1.2m HIGH ACCESS GATE DETAIL 1:20





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CONCEDUCTION ISSUE	ı
CONSTRUCTION ISSUE	
	l i
	-

	REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
	Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
				SHEET:	A3	
l				SCALE:		
	P8	PRELIMINARY ISSUE	23.04.24			

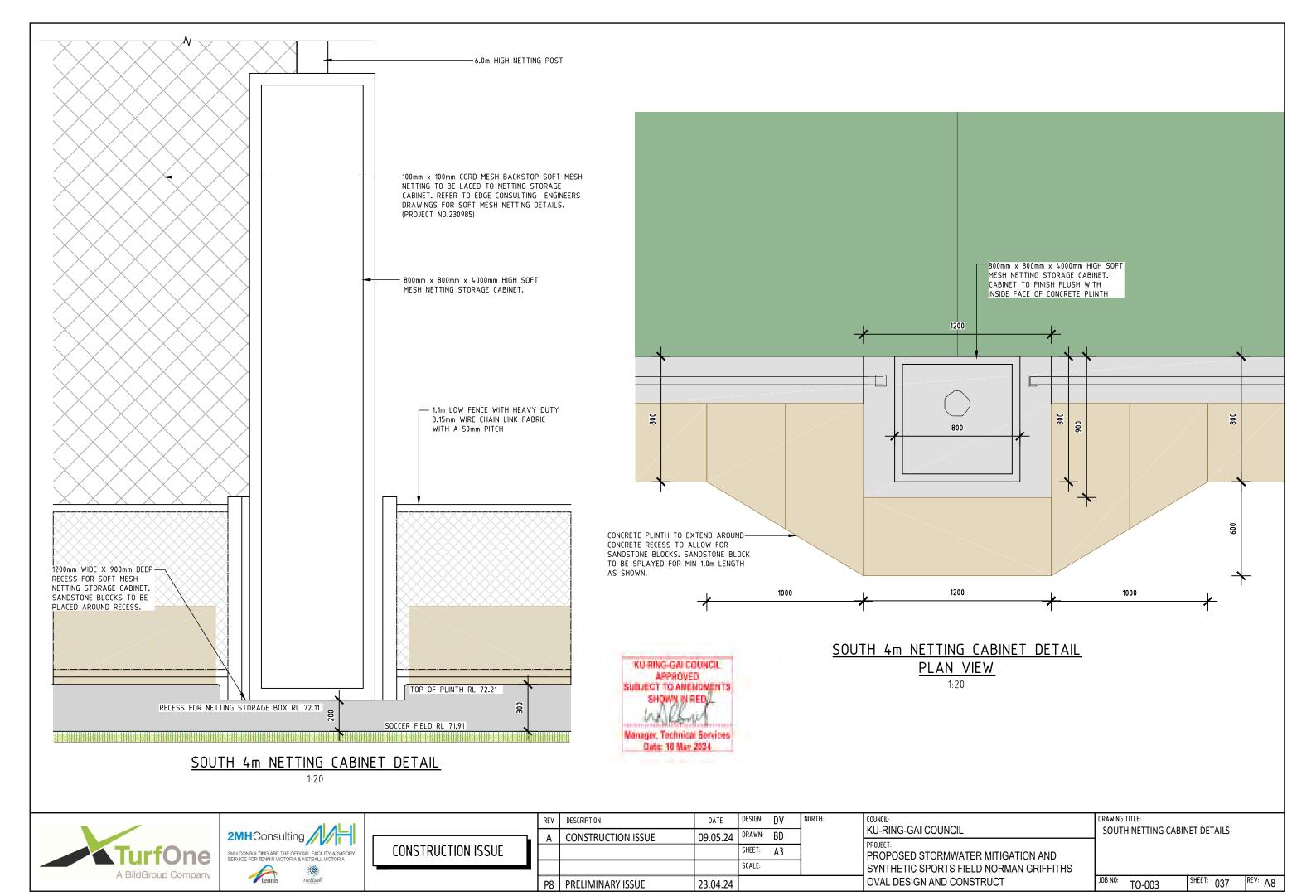
COUNCIL:	DRAWING
KU-RING-GAI COUNCIL	NORTI
PROJECT:	SOUTI
PROPOSED STORMWATER MITIGATION AND	
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS	
OVAL DESIGN AND CONSTRUCT	JOB NO:

DRAWING TITLE:

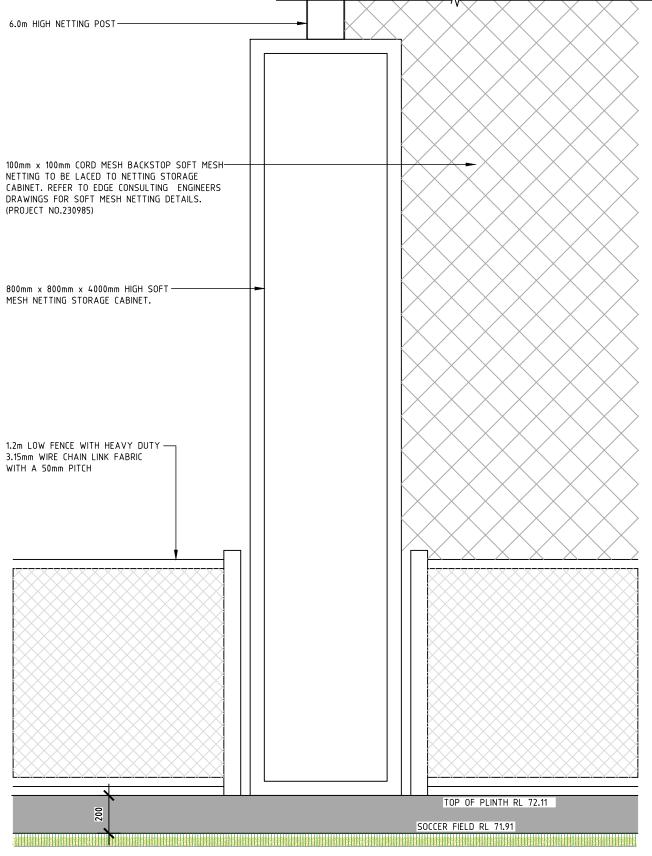
NORTH ACCESS GATE AND

SOUTH ACCESS GATE DETAILS

JOB NO: TO-003 SHEET: 036 REV: A8







NORTH 4m NETTING CABINET DETAIL

1:20





CONSTRUCTION ISSUE	
CONSTRUCTION ISSUE	

	REV	DESCRIPTION	DATE	DESIGN:	DV	NORTH:
L	Α	CONSTRUCTION ISSUE	09.05.24	DRAWN:	BD	
				SHEET:	A3	
				SCALE:		
	P8	PRELIMINARY ISSUE	23.04.24			

COUNCIL:	DRAWING 1	TITLE:
KU-RING-GAI COUNCIL	NORTH	H NETT
PROJECT:		
PROPOSED STORMWATER MITIGATION AND		
SYNTHETIC SPORTS FIELD NORMAN GRIFFITHS		
OVAL DESIGN AND CONSTRUCT	JOB NO:	TO-C

RTH NETTING CABINET DETAILS

SHEET: 038 JOB NO: TO-003

REV: A8



Appendix B – Stamped Civil Drawings and additional Reports



Norman Griffiths Oval

Flood Effect on EEC zone for 1% AEP Flood event



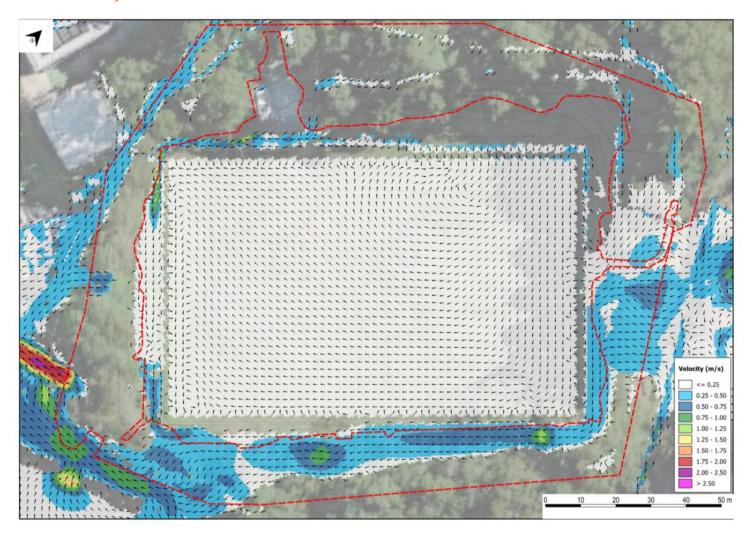
Hi Piran,
As requested, we have checked the flood extent occurring in the EEC zone



Flood Depth

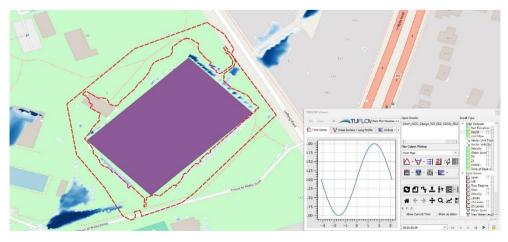


Flood Velocity

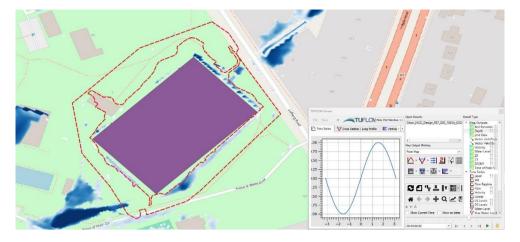


The 1% AEP flood (1 in 100 year event) affects the EEC area for about 50 minutes. . The 1% AEP flood overflow starts about 5 minutes after the storm commences and finishes after about 55 minutes after the storm commences.

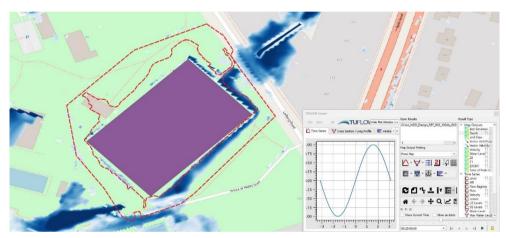
Depth Series



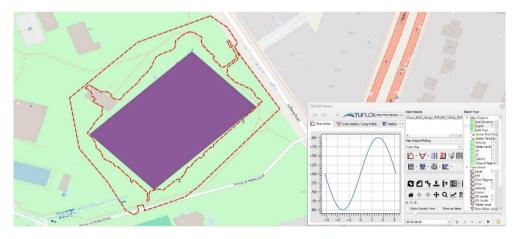
Depth 55min



Depth 40min

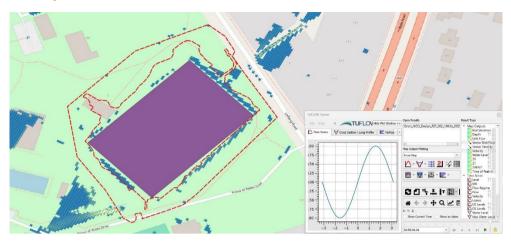


Depth 25min

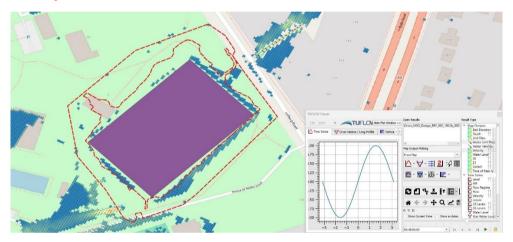


Depth 5min

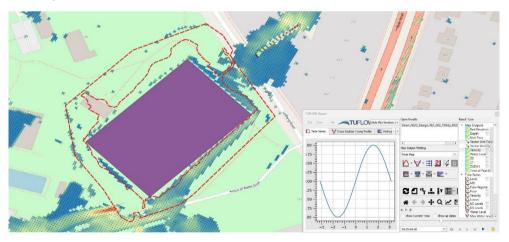
Velocity Series



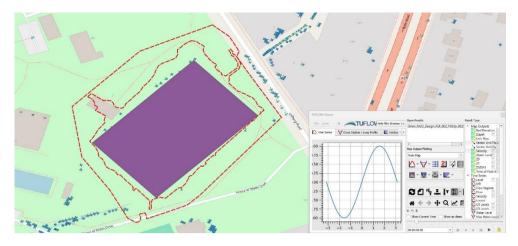
Velocity 55min



Velocity 40 Min



Velocity 25min



Velocity 5min

